

Automated re-prefabrication system for buildings using robotics

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Abstract

Prefabrication has the advantages of simplicity, speed and economy but has been inflexible to changes in design which is a primary reason behind its limited market share in the construction industry. To tackle this drawback, this study presents a Robotic Prefabrication System (RPS) which employs a new concept called “re-fabrication”: the automatic disassembly of a prefabricated structure and its reconstruction according to a new design. The RPS consists of a software module and a hardware module. First, the software employs the 3D model of a prefabricated structure as input, and returns motor control command output to the hardware. There are two underlying algorithms developed in the software module. First, a novel algorithm automatically compares the old and new models and identifies the components which the two models do not have in common in order to enable disassembly of the original structure and its refabrication into the new design. In addition, an additional novel algorithm computes the optimal refabrication sequence to transform one model into another according to the differences identified. Meanwhile, the hardware module takes the motor control commands as input and executes the appropriate assembly/disassembly operations, and returns the desired refabricated structure in real-time. Validation tests on two lab-scaled prefabricated structures

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23 demonstrate that the system successfully generated the desired refabrication sequences and
24 performed all assembly operations with acceptable placement precision.

25 **Key words:** Robotic Prefabrication System (RPS), Robotics, Prefabrication, Disassembly,
26 Refabrication

27 **1. Introduction**

28 In theory, most common construction components can be decomposed to a combination of
29 parts and connectors, such as bricks and cement, wooden slabs and mating joints, or girders
30 and bolts. It follows that most construction activities can be broken down into a series of
31 assembly operations to form larger and larger assemblies from individual parts. Over the last
32 few decades, individual elements, also called prefabricated components, have become popular
33 in the construction industry. Prefabrication is a construction practice which manufactures the
34 majority of building's sub-assemblies ranging from wall panels to complete rooms in a
35 controlled factory environment, before transporting the sub-assemblies to the construction site
36 for assembly [1]. Modular buildings and modular homes, which are recently getting more
37 popular in the construction industry, are a representative example of adopting the concept of
38 prefabrication [2]. Compared to site-cast (or in-situ) construction, precast concrete elements
39 offer faster production, lower cost, and more efficient assembly of elements [3]. For example,
40 it has been reported that replacing in-situ concrete casting panels with prefabricated elements
41 has resulted in a 70% reduction in construction time and a 43% reduction in labour cost [4].
42 Moreover, the use of precast concrete elements leads to a cleaner and safer construction
43 environment [4-5].

44 Despite these benefits, off-site construction methods are estimated to comprise only around 10%
45 of the construction market of UK [6]. There are numerous technical, financial and regulatory
46 barriers that contribute to such a slow adoption of prefabrication [7]. While the relative

47 prominence of most of these barriers is still open to debate, there seems to be a general
48 consensus within the industry as stated that “*The main disadvantages of prefabrication are*
49 *inflexibility to changes in design.*” [5]. This study focuses on tackling the main disadvantage
50 of prefabrication: the inflexibility of prefabrication to changes in design.

51 Current construction industry practice aims to increase flexibility by mass customization to
52 overcome the shortcoming [8]. This involves the mass production of certain core designs which
53 can later be customized using a catalogue of modules: a plain timber panel, for example, can
54 be switched for a panel with thermal insulation layers and window frame components pre-fitted.
55 This approach requires automation as a prerequisite since any change to the repetition of parts
56 slows down production until the entire process is fully automated, including assembly and not
57 just the making of the parts [2]. The need for an automated and mass-customisable construction
58 process thus motivates developments in the field of ‘robotic prefabrication’. It was argued that
59 the level of automation in making prefabricated building components using robots in the
60 precast concrete industry is high and this has mainly stemmed from the flexible production
61 system which could execute various tasks such as setting moulds and placing reinforcement
62 bars [9].

63 Even though mass customization using robotic fabrication has improved flexibility during
64 the design process, design changes such as those arising from inspection failures or changes in
65 customer requirements can no longer be incorporated once the design has been physically built.
66 Flexibility can thus be further improved if it becomes possible to *automatically disassemble a*
67 *prefabricated structure and reconstruct it according to a new design* - a concept which shall
68 be referred to from here onwards as “refabrication”.

69 Not only will a solution to this problem associated with automation and refabrication help
70 accentuate the benefits of prefabrication over bespoke construction and increase its market

71 share, but also it will boost productivity levels. It was reported that approximately 40% of
72 construction projects experience more than 10% change [10]. It was also estimated that
73 productivity will drop below the estimated level for projects with more than 20% change, and
74 conversely productivity will increase when change is effectively dealt with and kept below 5%
75 [10]. Based on the statistical productivity estimation in the previous study, development of a
76 solution with the capability of automated refabrication can increase the productivity as changes
77 in design can be addressed in a timely and effective manner. Moreover, this solution will
78 provide positive environmental impact: When subjected to customers' order changes or
79 inspection failures such as a joint failing under load or a component exceeding tolerance limit,
80 a modification of the original structure is much less wasteful than a complete demolition. In
81 this sense, an automated disassembly and refabrication solution in the prefabrication industry
82 can significantly contribute to the development of sustainable construction which attempts to
83 reuse the components and other resources needed for construction [11].

84 This study presents a new concept and demonstrates the idea to increase the flexibility of
85 prefabrication through the early development of a refabrication system using robotics. A
86 Robotic Prefabrication System (RPS) that employs a new concept "refabrication" is presented
87 here. The RPS consists of a software module and a hardware module which are detailed in
88 Section 3.

89 The rest of this paper is organized as follows. Section 2 reviews current state-of-practice
90 and state-of-research into robot-aided construction. The proposed system and its modules are
91 then presented in Section 3. Validation tests are conducted and the results are reported and
92 analysed in Section 4. Finally, conclusions are drawn and recommendations for future work
93 are discussed in Section 5.

94 **2. Related work**

95 It is often argued that the construction industry has the features of a loosely coupled system
96 which favours productivity in projects while innovation suffers [12]. A number of researchers
97 have also argued that the construction industry has failed to adopt techniques that have
98 improved performance in other industries such as just-in-time [13] and ‘industrialization’ of
99 manufacturing processes [14]. In this regard, the construction industry particularly in the
100 prefabrication sector needs to revolutionize by embracing such advanced automation
101 techniques and systems. This section presents related studies and attempts that has been made
102 so far regarding robotic based automation in the construction industry to identify the needs and
103 gaps in knowledge in the current prefabrication domain.

104 **2.1. Robot-aided automated construction in the building industry**

105 Over the past few decades, automation systems using robot technologies has been less
106 favourably developed and applied in the construction and building industry compared to the
107 industrial and the manufacturing industry because of the dynamic and uncertain environments
108 of the industry [8, 15]. In an attempt to automate repetitive construction processes and increase
109 the productivity in construction, several robotic systems such as slab finishing robot system
110 and concrete formwork cleaning robot system, were developed in the 1980s [16-17].
111 Skibniewski also conducted the feasibility study on selected construction industry processes
112 in order to examine the possibility of using robots in the future construction industry [16].
113 During the 1990s, Japanese companies and universities led the R&D activities in the field of
114 robot-aided automated construction and the focus was the development of new robotic systems
115 and the automation of existing machinery [9]. These robots developed for house buildings tried
116 to automate certain construction processes such as layering bricks, constructing building walls
117 and facades [18-21]. However, the ‘bubble economy’ crisis in Japan had reduced investment in
118 the research area, and only few construction robots had succeeded in the market. As the result

119 of the risk of high initial cost and the unsatisfactory return on investment, construction industry
120 had continued to be conservative in “tomorrow’s construction robots” [8].

121 Regarding the recent development of construction robots for buildings, there are some
122 commercial systems available in the market such as SAM [22], Contour Crafting [23] and
123 Oversize 3D printing systems [24]. SAM is a semi-automated mason robotic bricklayer and
124 has a function of laying about 800 to 1,200 bricks a day while a human mason can lay about
125 300 to 500 bricks a day. This robot, however, still requires a human construction worker to tidy
126 up the mortar and place bricks in difficult area such as corners. Another innovative
127 development named Contour Crafting is a layered fabrication system designed for automating
128 the construction of whole structures. This system, however, has not reached the stage of
129 constructing a complete housing or building with a satisfactory accuracy. D-shape is a large
130 3D printer that uses a layer-by-layer printing process to create stone-like objects. It is reported
131 that the printer still needs to be further developed in order to make larger and more complex
132 buildings [24].

133 In addition to the commercial systems mentioned above, several academic studies have
134 been conducted. Choi et al. [25] developed a construction robot using pneumatic actuator and
135 servo motor to support construction workers in mounting window glasses or fixing panels. A
136 cable-robot system called ‘SPIDERobot’ was also developed to perform assembly operations
137 in on-site architectural construction [26]. Chu et al. [27] presented the development of a robotic
138 beam assembly system consisting of a robotic bolting device that performs the main function
139 for the beam assembly work and a robotic transport mechanism that transports the robotic
140 bolting device to target bolting positions around a building under construction. However, it
141 seems that the recent studies have focused on development of robot systems with the purpose
142 of automating the construction or maintenance tasks, which has limitations in overcoming the
143 inflexibility problem mainly occurred in the design and manufacturing phase of a project.

144 **2.2. Robotic prefabrication in the building industry**

145 Robotic systems have been mainly employed in the prefabrication construction industry for
146 the production of modular and prefabricated housing components such as ceilings, walls and
147 roofs. Bock [17] detailed a robotic precast concrete panel factory that utilizes a multi-functional
148 formwork unit which allows flexible production of concrete floors, walls and roof panels. In
149 this factory, a precast manufacturing system, which integrates CAD with Computer-Aided
150 Manufacturing (CAM), controlled concrete distributor to spread the right amount of concrete
151 by taking into account the geometric position of window or door openings according to CAD
152 layout.

153 Three primary projects which illustrate the advances and the state of the art of the robotic
154 prefabrication in the building industry are: (1) ROCCO [18], (2) FutureHome [19-20], and (3)
155 ManuBuild [21].

156 ROCCO [18] features two different robotic systems: one for erection of walls in residential
157 buildings with a reach of 4.5m and a payload of 400kg, and one for industrial buildings with a
158 reach of 8.5m and a payload of 500kg. It includes a software system that assists engineers in
159 wall partitioning, layout planning and logistics planning. The system is also capable of
160 automatically generating manufacturing commands and robot assembly tasks to produce
161 prefabricated elements.

162 FutureHome [19-20] aims to build fully-manufactured houses instead of only prefabricated
163 parts. The hardware now features both an off-site production plant and on-site assembly plant,
164 with a robotized gantry crane to perform on-site assembly tasks. The software system,
165 AUTOMOD3, generates assembly sequences and motion paths for robots to automatically
166 carry out the construction process. It also provides a simulation tool to allow the assembly
167 process to be visualized and inspected before execution.

168 ManuBuild [21] facilitates the adoption of mass customization in the construction industry.
169 This project targets a breakthrough from a “craft and resource-based construction” industry
170 into an “open and knowledge-based manufacturing” industry, leading to not only make
171 buildings as open systems equipped with flexible and scalable components but also offer
172 customers increased choice and design flexibility.

173 Recently, the group of Gramazio Kohler Research at ETH Zurich have developed numerous
174 automated robot systems including a mobile robotic brickwork system [28] and an aerial
175 robotic construction system [29]. These studies are recognized as a meaningful contribution to
176 the additive non-standard fabrication for the assembly of building components.

177 **2.3. Robotic disassembly and reconstruction**

178 Nevertheless there have been academic and practical studies aiming to develop robotics-
179 based automated assembly systems as investigated in Sections 2.1 and 2.2, it has been found
180 that there is still no study available dealing with automated disassembly and reconstruction of
181 prefabricated structures in the construction industry. In order to tackle this limitation in the
182 current prefabrication industry, a new system that provides the capability of automated
183 disassembly and refabrication was proposed in this study. This study adopts the most common
184 assembly planning strategy ‘assembly-by-disassembly’. This is because (1) when only
185 geometric constraints are considered, an invertible disassembly sequence always leads to a
186 feasible assembly sequence; and (2) a structure in its assembled state has many more
187 constraints than in its disassembled state, which results in a smaller search space for the planner
188 [30-32]. For this reason, knowledge from the field of automated product assembly, which has
189 been widely researched since the late 1980s, is directly relevant to the disassembly and
190 refabrication of prefabricated structures.

191 The core algorithmic parts of the automated product assembly include geometrical
192 reasoning in assembly planning [33], stability analysis of assemblies [34] and assembly
193 sequencing using a path planning approach [31]. Recently, Rakshit and Akella [35] combined
194 stability and geometric constraints analysis to produce an algorithm capable of simulating the
195 entire assembly sequence by taking into account physical forces and part motion. This
196 algorithm is outlined below:

197 ***Assumptions:***

- 198 - The sequence is two-handed and monotone
- 199 - Each part is moved by a gripper at constant velocity with perfect position control
- 200 - Part movement is modelled as quasi-static motion with finite translations
- 201 - Collision of gripper with assembly is not considered

202 ***Geometric analysis:***

- 203 - Firstly, an enumeration of all possible sequences is generated using AND/OR graph [30]
- 204 - Secondly, geometrically feasible sequences are filtered out using Non-Directional
205 Blocking Graph [36]

206 ***Stability analysis:***

- 207 - For frictionless cases, calculation of the relative movement in terms of the relative
208 acceleration between the parts in the assembly [37] is conducted
- 209 - For cases with friction, Baraff's method [37] becomes ineffective and a different set of
210 complementary constraints must be used [38]

211 **2.4. Gaps in knowledge and scope of this study**

212 Even though the state-of-the-art algorithm developed by Rakshit and Akella [35] can be
213 used to generate a stable disassembly sequence for the majority of common structural
214 assemblies, this is only part of what is needed to realize the concept of "refabrication" which

215 also requires the refabrication sequence based on a new design. Therefore, the objective of this
216 study is to develop a RPS of prefabrication that provides the automatic disassembly and
217 reconstruction of a prefabricated structure. The concept is demonstrated using an automated
218 robotic system operating on a small-scale structure to provide the first stepping stone for future
219 researchers working towards the final goal: refabrication of arbitrary full-scaled structures.

220 Refabrication is an extension of the general assembly planning problem, which includes
221 many sub-problems such as connector design and manipulation, feeder and tool selection,
222 assembly sequencing, and robot path planning. However, since this study focuses on proving
223 the proof-of-concept of the RPS as a first stepping stone, a full treatment of all aspects above
224 is beyond the scope of this work. The simplifications made in this study are:

- 225 - The robot arm can only move in 2D (a vertical plane with respect to the ground)
- 226 - The path planner¹ produces collision-free but non-optimal paths
- 227 - The assembly sequencer² only takes into account:
 - 228 + “Stacking” operations (pure translations and no rotation)
 - 229 + Geometric constraints (ignore stability constraints)
 - 230 + Two-handed monotone assemblies.
- 231 - Only two types of connectors were considered:
 - 232 + Null connectors: where two parts are kept in contact purely by gravity (e.g. Jenga
 - 233 blocks)
 - 234 + Permanent connectors: where two parts are connected through a joint which is
 - 235 impractical to undo after the assembly operation is completed (e.g. cemented bricks).

¹ A path planner calculates paths in space that a robot arm can take to execute a specific assembly sequence. These paths are often subject to a certain set of constraints, such as collision-free or optimal-time.

² An assembly sequencer produces a set of assembly operations and constraints on their ordering. Each operation specifies a motion that combines two or more subassemblies to form a larger assembly. Any ordering of operations that obey the sequence constraints is called an assembly sequence.

236 **3. Development of Robotic Prefabrication System**

237 **3.1. System design**

238 **3.1.1. Top level**

239 The RPS is designed with the capability of automatically building a 3D structure given its
240 digital model, as well as of deconstructing obsolete parts and updating the original structure
241 given a new design. This capability can be divided into two main functions, which are
242 ‘assemble’ and ‘refabricate’ as illustrated in Figure 1. When the RPS implement the ‘assemble’
243 function, the digital 3D model of a structure and raw material are fed into the RPS as inputs
244 and a 3D structure is assembled according to the original design. Meanwhile, when a new 3D
245 model comes into the RPS due to a change in design, the RPS implements the tasks of
246 disassembly and reconstruction according to the new design and finally results in a new 3D
247 structure.

Insert Figure 1 approximately here

248

249 **3.1.2. Second level**

250 The RPS includes both a software module and a hardware module to meet top-level
251 functional requirements. The software module takes digital inputs and gives motor control
252 commands to the hardware module, while the hardware module takes the motor control
253 commands, manipulates the physical inputs, and returns physical outputs. In addition, to carry
254 and update information about motor states, a feedback loop from the hardware module to the
255 software module is included.

256 **3.1.1 Third level**

257 For the software module, there are four software sub-modules needed to carry out the
258 second-level function described above. Figure 2 illustrates the workflow of the software
259 module. The functions of each software sub-module are described as follows:

- 260 - *Model analyser*: Analyses an input 3D model and returns the its geometric data, such as the
261 size, shape and position of its individual parts.
- 262 - *Models comparator*: Takes in geometric data from two different 3D models, identifies all
263 those individual parts which the two models do not have in common, and returns the
264 geometric data of these parts.
- 265 - *Assembly sequencer*: Takes in geometric data of the entire model or set of specific parts,
266 depending on which top-level function the RPS needs to execute, returns the appropriate
267 (dis)assembly sequences.
- 268 - *Hardware controller*: Takes in (dis)assembly sequences and generates a set of motor
269 control commands such that the hardware will carry out the appropriate (dis)assembly
270 operations and create the desired 3D structure. The controller also needs to take in the
271 feedback signal containing the motor states from the hardware module, in order to
272 synchronize the execution of motor control commands.

Insert Figure 2 approximately here

273 More details of the design of the software sub-modules are presented in Section 3.3.

274 Since the task of the hardware module is common to many existing assembly systems in
275 industry, different types of systems were investigated to pick out one as a suitable template.
276 However, due to the limited variety of components available for construction of the hardware
277 system as well as the large number of motors required, it became clear that assembly design
278 typically employed in industry was impractical to pursue in this study. Therefore, a basic
279 hardware module was designed specifically for this study to fulfil our objectives. Figure 3
280 shows the hardware module designed in this study. The hardware module comprises four sub-
281 modules:

- 282 - *Gripper*: Securely holds a raw material block during its transportation from stock side to
- 283 assembly side, and vice versa.
- 284 - *Lift drive*: Enables vertical translation of the gripper
- 285 - *Forward drive*: Enables longitudinal translation of the gripper
- 286 - *Support structure*: Provides an elevated runway for the forward drive on top, as well as
- 287 stock space and assembly space at the bottom

Insert Figure 3 approximately here

288 More details of the design of the hardware sub-modules are presented in Section 3.4.

289 **3.2. Choice of materials**

290 Two constituent component options were considered for the choice of materials for this
291 study:

- 292 - Fully-customized components: Structural components could be designed using CAD
- 293 software packages, then either machined or manually created in a workshop. This enables
- 294 great flexibility in design, but it is relatively time and cost demanding during the
- 295 manufacturing and construction of the components.
- 296 - Standardized components: Structural components could be built directly out of LEGO
- 297 Duplo block and LEGO Mindstrom [39] components. Actuators are also available as
- 298 servo motors from the LEGO Mindstorms set. This gives limited flexibility in design, but
- 299 requires relatively little time during the construction of the sub-modules.

300 The use of standardized components to construct the entire hardware module can act as
301 supporting evidence for the philosophy advocated in this study that many structures can be
302 efficiently constructed through the assembly of modular components. For this reason, it was
303 decided that the hardware module would be constructed entirely out of LEGO Duplo and
304 LEGO Mindstorm components. This reasoning also applied to the choice of building block

305 used as input raw material to the hardware module; LEGO Duplo and Jenga blocks were
306 therefore chosen. Since Jenga blocks are held in contact by gravity alone, and Duplo blocks
307 are held in contact by fairly sturdy male-female connectors, they here represent null and
308 permanent connectors, respectively.

309 **3.3. Software module**

310 **3.3.1. Model analyser**

311 The model analyser is built to analyse an input 3D model and return the model' geometric
312 data. Since the 3D structures which our system operates on are cuboid, the geometric data
313 extracted are: (1) The coordinates of each component's centroid, (2) The size of each
314 component's bounding box (width, length and height), and (3) The ID of each component
315 (which must contain the string "Lego" or "Jenga" so that the type of connector it possesses can
316 be later inferred).

317 Having identified the output requirements above, an algorithm was developed to take in a
318 file of 3D model and return an array containing three variables {id, boundBoxSize, centrePoint}
319 (see *Algorithm 1*).

320 Let $\langle C \rangle$ be an array containing individual components found in the input 3D model and $\langle G \rangle$
321 be an array representing the geometric data of the components:

322 *Algorithm 1: Model analyser*

323 Input: A 3D model file, e.g. 'model.ifc'

```
324 1:  do  $\langle C \rangle = \text{ReadModel}()$ ;  
325 2:  if  $\langle C \rangle == \emptyset$  then  
326 3:      return NO COMPONENT FOUND  
327 4:  end if  
328 5:  for each C in  $\langle C \rangle$  do  
329 6:      G.id = C.GetName();  
330 7:      G.boundBoxSize = C.GetSize();  
331 8:      G.centrePoint = C.GetCentroid();  
332 9:       $\langle G \rangle.$ Add (G);
```

```
333 10:   end for each  
334 11:   return <G>
```

335 3.3.2. Model comparator

336 The role of the model comparator is to take in geometric data of two different 3D models,
337 identify all individual parts which the two models do not share in common, and return the
338 geometric data of such parts. A function was created to do the tasks. It takes in two arrays
339 containing the geometric data of two different 3D models, loops through each member of the
340 first array, and checks if it also exists in the second array. Finally, it returns an array containing
341 all members of the first array that do not exist in the second array. However, this function itself
342 only returns true if the pair of array members being compared have the exact same variables
343 (i.e. fully identical). This means that given two 3D models which are identical in every aspect
344 except their position in space (i.e. partially identical), the models comparator will conclude that
345 these two models have zero common parts.

346 In order to tackle this issue, a new function that helps align the coordinates of the two input
347 models was created. It is, however, a non-trivial problem to align two arbitrarily different
348 models such that the alignment should lead to as few refabrication operations as possible. It is
349 also impractical to attempt every possible alignment of large models since the number of
350 checks is proportional to N^2 , where N is the number of partially identical parts and determined
351 from a brute-force alignment approach. Hence, assuming that it is focused on prefabrication of
352 building walls and the majority of design changes are either wall extensions while keeping the
353 door/window positioning or repositioning of door/window while keeping the wall dimensions,
354 the number of alignments attempted can be limited to three: (1) Alignment of lower left corner,
355 (2) Alignment of lower right corner, and (3) Alignment of door feature. Three sub-functions
356 were thus developed: ‘AlignLeft()’, ‘AlignRight()’ and ‘AlignDoor()’.

357 Let $\langle G1 \rangle$ and $\langle G2 \rangle$ be arrays representing the geometric data of components from two
 358 different 3D models; $\langle G2L \rangle$, $\langle G2R \rangle$ and $\langle G2D \rangle$ be arrays representing the geometric data of
 359 components from the second model after left, right and door alignment respectively; and $\langle L \rangle$,
 360 $\langle R \rangle$ and $\langle D \rangle$ be arrays representing not-in-common components between $\langle G1 \rangle$ and $\langle G2L \rangle$,
 361 $\langle G2R \rangle$, $\langle G2D \rangle$ respectively:

362 **Algorithm 2: Model Comparator**

363 Input: $\langle G1 \rangle$, $\langle G2 \rangle$

```

364 1:  do  $\langle G2L \rangle = \text{AlignLeft}(G2)$ ;
365 2:  do  $\langle G2R \rangle = \text{AlignRight}(G2)$ ;
366 3:  do  $\langle G2D \rangle = \text{AlignDoor}(G2)$ ;
367 4:  foreach  $G1$  in  $\langle G1 \rangle$  do
368 5:      if  $\langle G2L \rangle.\text{Contains}(G1) == \text{false}$  then
369 6:           $\langle L \rangle.\text{Add}(G1)$ ;
370 7:      end if
371 8:      if  $\langle G2R \rangle.\text{Contains}(G1) == \text{false}$  then
372 9:           $\langle R \rangle.\text{Add}(G1)$ ;
373 10:     end if
374 11:     if  $\langle G2D \rangle.\text{Contains}(G1) == \text{false}$  then
375 12:          $\langle D \rangle.\text{Add}(G1)$ ;
376 13:     end if
377 14: end foreach
378 15: return  $\langle L \rangle$ ,  $\langle R \rangle$ ,  $\langle D \rangle$ 

```

380 Note that since the model comparator does not have the capability to evaluate the number
 381 of refabrication operations required as a result of model alignment, it must pass on the
 382 geometric data of not-in-common parts for all three alignment scenarios to the next sub-module,
 383 the ‘Assembly sequencer’.

384 3.3.3. Assembly sequencer

385 The assembly sequencer can execute two functions, “Assemble” and “Refabricate”. If the
 386 system is executing the “Assemble” function, the assembly sequencer takes in the geometric
 387 data of the components previously extracted from the 3D model, and returns the appropriate

388 sequence of assemblage. Since it is already assumed that all raw material blocks are cuboids,
389 an effective stack-assembly sequencing algorithm is as follows:

- 390 - Search through all members of the input array containing geometric data
- 391 - Sort the members in ascending order according to the distance between ground and each
392 member's bottom bound line
- 393 - Then proceed to sort the members in descending order according to the distance between
394 the stock side and each member's right-hand-side bound line

395 This algorithm will thus return an array whose members are indexed in such a way that the
396 building blocks will be assembled from the bottom layer up and from the far end of the
397 assembly side towards the stock side. This is illustrated in Figure 4.

Insert Figure 4 approximately here

398 Let $\langle G \rangle$ be an array representing a set of all components of a 3D model and its geometric
399 data; $\langle S \rangle$ be an array representing the same components now indexed according to the desired
400 assembly sequence; and $\langle \text{bottomBoundLine} \rangle$ and $\langle \text{rightBoundLine} \rangle$ be arrays containing the
401 position of the bottom and right bounds of the components' geometry:

402 **Algorithm 3:** *Assembly Sequencer (executing the "Assemble" function)*

403 Input: $\langle G \rangle$

```
404 1:  foreach G in  $\langle G \rangle$  do  
405 2:      bottomBoundLine = G.centrePoint.Y - G.boundingBoxSize.Y ÷ 2  
406 3:      rightBoundLine = G.centrePoint.X + G.boundingBoxSize.X ÷ 2  
407 4:       $\langle \text{bottomBoundLine} \rangle$ .Add(bottomBoundLine)  
408 5:       $\langle \text{rightBoundLine} \rangle$ .Add(rightBoundLine)  
409 4:  end foreach  
410 5:  do  $\langle S \rangle = \langle G \rangle$ .OrderBy( $\langle \text{bottomBoundLine} \rangle$ ).ThenByDescend( $\langle \text{rightBoundLine} \rangle$ )  
411 6:  return  $\langle S \rangle$ 
```

412 If the system is executing the "Refabricate" function, the purpose of the assembly
413 sequencer is to take in the geometric data of not-in-common parts for all three alignment

414 scenarios outlined above, evaluate which alignment is the most optimal, then return the
415 appropriate “refabrication sequence”. Here, the most optimal alignment is defined here as *the*
416 *alignment which results in the minimum number of (dis)assembly operations required to*
417 *refabricate the existing structure* and this in turn begs the question on *how can one calculate*
418 *the number of (dis)assembly operations required?* This question can be answered using the
419 Non Directional Blocking Graph (NDBG) technique developed by Wilson [33]. This technique
420 involves three main steps: Step 1 - the construction of directional blocking graphs (DBGs),
421 where each one indicates which parts within the assembly would collide given an instantaneous
422 displacement in a particular direction; Step 2 - the partitioning of space into regions which
423 share the same DBG; Step 3 - the combination of all DBGs to form the NDBG.

424 However, since this technique can be applied to assemblies of arbitrary polygons and
425 accounts for arbitrary linear motion in 3D space, it is too generalized for the purposes of this
426 study. Consequently, a stripped-down version of the NDBG technique was used to develop the
427 assembly sequencer. Figure 5 provides an example illustrating how the NDBG technique can
428 be simplified when all (dis)assembly operations are restricted to 2D stacking operations:

- 429 - The left hand side is an example stack assembly consisting of four subassemblies, P1, P2,
430 P3 and P4.
- 431 - The top right side shows the DBG whose nodes represent the subassemblies and where
432 each outgoing arrow indicates an expected collision when given an instantaneous
433 displacement in the vertically upwards direction. Since vertically upwards is the only
434 direction allowed for disassembly operations, the NDBG is the same as the DBG and steps
435 2 and 3 of the NDBG algorithm can be skipped.
- 436 - The bottom right side represents the DBG as a matrix. The matrix rows and columns
437 represent all possible origin and destination nodes of DBG, while the elements 0 and 1 of
438 the matrix represent the absence or presence of all possible DBGs.

Insert Figure 5 approximately here

439

440 In order to calculate the number of disassembly operations required for any chosen sub-
441 assembly, the values of the matrix elements must first be determined and the optimal
442 disassembly sequence be deduced. The values of matrix elements are determined using a
443 function called ‘CalcDBG()’ which takes an array with N members containing geometric
444 information of the assembly, and returns an N by N matrix which represents the DBG of the
445 assembly.

446 The algorithm implemented is outlined below:

- 447 1. Create an N by N matrix with all elements set to zero
- 448 2. For each subassembly (denoted as A), check the bounding box of any other
449 subassembly (denoted as B) and see if both of the following conditions are satisfied:
- 450 ○ The top line of the bounding box of A is at the same height as the bottom line of the
451 bounding box of B.
 - 452 ○ The bounding box of B lies in the “collision zone”, which is defined as the 3D space
453 covered by the bounding box of A when extended in the vertical direction.
- 454 If yes, change the appropriate matrix element to one.
- 455 3. Terminate when step 2 has been performed for all subassemblies.

456 Let <G> be an array representing all components and their geometric data from a 3D model;
457 and dbg[] be a matrix which represents the DBG of the same model:

458 **Algorithm 4:** *Function CalcDBG()*

459 Input: <G>
460 1: **do** N = <G>.GetLength()
461 2: **do** dbg[] = NewZeroMatrix(N, N)
462 3: **for** i = 1, 2...N **do**
463 4: **for** j = 1, 2...N **do**

```

464 5:           if GjBottomLine == GiTopLine then
465 6:               if Collision (Gi, Gj) == true then
466 7:                   dbg [i,j] = 1
467 8:               end if
468 9:           end if
469 10:        end for
470 11:    end for
471 12:    return dbg

```

472

473 Note that the above function is based on the original DBG technique, which assumes that all
474 subassemblies are free-flying and held together via null connectors. However, since our system
475 operates on assemblies with the presence of permanent connectors, another function called
476 ‘CalcTruncatedDBG()’ was generated. This function takes the N by N matrix produced by the
477 CalcDBG() function and returns a M by M matrix, where M = (N - the number of permanent
478 connectors), using the algorithm below:

- 479 1. Find all matrix rows which contain “1” element
- 480 2. For each row found in step 1, check the following cases of its “1” elements:
 - 481 ○ If the two subassemblies involved are not held together by a permanent connector,
482 skip to the next “1” element.
 - 483 ○ Otherwise, perform the following operations on the rows and columns which
484 represent two subassemblies involved (here denoted as A and B):
 - 485 + Combine column of B and column of A using Boolean OR
 - 486 + Combine row of B and row of A using Boolean OR
 - 487 + Set all elements on the matrix diagonal to zero
- 488 3. Terminate when step 2 has been performed on all rows

489 Let <G> be an array representing all components and their geometric data from a 3D model
490 and let dbgTrunc[] be a matrix which represents the truncated DBG of this 3D model:

491 *Algorithm 5: Function CalcTruncatedDBG()*

```

492 Input: <G>
493 1:  do N = <G>.GetLength()
494 2:  do dbgTrunc[,] = CalcDBG(<G>)
495 3:  for i = 1, 2...N do
496 4:      for j = 1, 2...N do
497 5:          if dbgTrunc[i,j] = 1 then
498 6:              if PermCon (Gi, Gj) == true then
499 7:                  combineOR(dbgTrunc[i,*], dbgTrunc[j,*])
500 8:                  combineOR(dbgTrunc[* ,i], dbgTrunc[* ,j])
501 9:                  dbgTrunc[i,i] = dbgTrunc[j,j] = 0
502 10:             end if
503 11:         end if
504 12:     end for
505 13: end for
506 14: return dbgTrunc

```

507 An illustrative example of a transformation from the DBG matrix shown in Figure 5 to a
508 new truncated DBG matrix is provided in Figure 6.

Insert Figure 6 approximately here

509 Once all matrix elements are calculated, the optimal disassembly sequence for any chosen
510 subassembly are determined using a function called GetDisassemblyTree(). This function takes
511 in three pieces of information, (1) an array with N members containing the geometric
512 information of the assembly, (2) the M by M matrix produced by the CalcTruncatedDBG()
513 function and (3) the geometric information of the subassembly that needs to be removed, and
514 then returns an array with L members where L = the number of subassemblies that need to be
515 removed as a consequence. Members of the output array contain the geometric information of
516 the to-be-removed subassemblies and the ordering of these members represents the sequence
517 in which they need to be removed. The implemented algorithm is as follows:

- 518 1. Jump to the matrix row corresponding to the subassembly that needs to be removed
519 from the overall assembly, here denoted as subassembly A.
- 520 2. Search the current row for “1” elements:
 - 521 o If one or more “1” elements are found, go to step 3.

- 522 ○ Otherwise, add the subassembly to disassembly tree and check:
- 523 + If the added subassembly is not A, go to step 4.
- 524 + Otherwise, terminate the algorithm.
- 525 3. Jump to the row whose index is equal to the column index of one of the “1” elements
- 526 found in step 2, and repeat step 2.
- 527 4. Jump to the row visited immediately before the current row, and repeat step 2.

528 Let <G> be an array representing all components and their geometric data from a 3D model;

529 dbgTrunc[] be a matrix which represents the truncated DBG of the 3D model; G* be a

530 representation of the component to be removed from the 3D model; and <T> be an array

531 representing the disassembly tree:

532 **Algorithm 6:** *Function GetDisassemblyTree()*

533 Input: <G>, G*, dbgTrunc[,]

534 1: **do** N = <G>.GetLength()

535 2: **do** index = CorrespondingRow (G*, dbgTrunc[,])

536 3: i = index

537 4: **if** GetCountOnes(dbgTrunc[index,*]) > 0 **then**

538 5: **for** j = 1, 2...N **do**

539 6: **if** dbgTrunc[i,j] = 1 **then**

540 7: i = j

541 8: JUMP TO LINE 4

542 9: **end if**

543 10: **end for**

544 11: **end if**

545 12: **if** GetCountOnes(dbgTrunc[index,*]) == 0 **then**

546 13: <T>.Add(G_i)

547 14: **if** i ≠ index **then**

548 15: i = GetPreviousI(i)

549 16: JUMP TO LINE 4

550 17: **end if**

551 18: **if** i = index **then**

552 19: **return** <T>

553 20: **end if**

554 21: **end if**

555

556 Using this algorithm on the example in Figure 5, a request to remove P3 will return the
557 disassembly tree in the form of an array {P1, P2+4, P3}.

558 Now the optimal disassembly sequence can be calculated for any chosen subassembly and
559 the three arrays returned by the ‘Model Comparator’ sub-module can finally be evaluated. A
560 function ‘GetDisassemblyForest()’ was generated to compute the optimal alignment and return
561 the optimal disassembly sequence, which is outlined below:

- 562 1. For each of the three input arrays:
- 563 - Calculate the disassembly tree for each array member using GetDisassemblyTree()
 - 564 - Concatenate all disassembly trees and remove duplicated members to obtain a new
565 disassembly sequence, here denoted as a “*disassembly forest*”
 - 566 - Count the members of the disassembly forest
- 567 2. Compare the three counts obtained from step 1 and choose the alignment type which
568 resulted in the lowest count.
- 569 3. Return the disassembly forest associated with the alignment type chosen in step 2

570 Let <L>, <R> and <D> be arrays representing not-in-common components returned by the
571 ‘Model Comparator’ sub-module; <fL>, <fR> and <fD> be arrays representing the
572 disassembly forests resulting from the three alignment scenarios:

573 **Algorithm 7: Function GetDisassemblyForest()**

```
574 Input: <L>, <R> and <D>
575 1:  foreach L in <L> do
576 2:      <fL>.Add( GetDisassemblyTree(L))
577 3:      <fL>.RemoveDuplicates()
578 4:  end foreach
579 5:  do countLeft = <fL>.GetLength()
580 6:  foreach R in <R> do
581 7:      <fR>.Add( GetDisassemblyTree(R))
```

```

582 8:         <fR>.RemoveDuplicates()
583 9:     end foreach
584 10:    do countRight = <fR>.GetLength()
585 11:    foreach D in <D> do
586 12:        <fD>.Add( GetDisassemblyTree(D))
587 13:        <fD>.RemoveDuplicates()
588 14:    end foreach
589 15:    do countDoor = <fD>.GetLength()
590 16:    do minCount = GetMinimum(countLeft, countRight, countDoor)
591 17:    if minCount = countLeft then
592 18:        return <fL>
593 19:    end if
594 20:    if minCount = countRight then
595 21:        return <fR>
596 22:    end if
597 23:    if minCount = countDoor then
598 24:        return <fD>
599 25:    end if

```

601 The original model with all the not-in-common subassemblies removed can now be compared
602 with the new model and the assembly sequence required to transform the former to the latter
603 can be computed. This is done using the ‘GetReassemblyForest()’ function which utilises the
604 following algorithm:

- 605 1. Subtract the array representing the disassembly forest from the array representing the
606 original model
- 607 2. Subtract the array obtained in step 1 from the array representing the new model
- 608 3. Compute an assembly sequence for the subassemblies contained in the output array of
609 step 2 using the AssemblySequencer() function, here denoted as “*reassembly forest*”

610 Let <GOrg> and <GNew> be arrays representing components from the original and the new
611 3D model respectively; <F> be an array representing the optimal disassembly forest returned
612 by the GetDisassemblyForest() function; and <R> be an array representing the optimal
613 reassembly forest:

614 **Algorithm 8:** Function *GetReassemblyForest()* ()

```
615 Input: <GOrg>, <GNew>, <F>
616 1:    do <R> = AssemblySequencer( <GNew> - <GOrg> + <F>)
617 2:    return <R>
```

619 Finally, the “disassembly forest” and “reassembly forest” obtained above are concatenated
620 to produce the desired *refabrication sequence* at the output.

621 3.3.4. Hardware controllers

622 The purpose of the hardware controller is to take in assembly/refabrication sequences and
623 generate a set of motor control commands such that the hardware will carry out the appropriate
624 assembly/refabrication operations and create the desired 3D structure. The controller also needs
625 to take in the feedback signal from the hardware module which contains motors’ states in order
626 to synchronize the execution of motor control commands. Note that the hardware controller
627 incorporated an open-source library called “MindSqualls” [40], which acts as the interface
628 between the C# .NET environment and the microcontroller of the Lego Mindstorm kit. This
629 sub-module also incorporated an open-source program called “Motor Control” developed by
630 [41], which implements algorithms that lead to more precise motor movements compared to
631 those produced by the native LEGO Mindstorm firmware.

632 3.4. Hardware module

633 Regarding the design of gripper sub-module, there are two main types of grasping profiles,
634 namely (1) Encompassing grasp: Where the gripper provides an enclosure to secure the object;
635 and (2) Frictional grasp: Where the contact surfaces generate friction to secure the object. Since
636 the purpose of our gripper is to securely hold a Lego Duplo/Jenga block during its
637 transportation from stock side to assembly side, an encompassing grasp would not be suitable
638 as it would prevent direct contact between the block and the structure, making it difficult to
639 achieve a precise stack operation. Hence, as for the grasp selection, a frictional grasp with flat
640 plates was chosen as the gripper mechanism to generate the required contact surface area.

641 Meanwhile, since servo motors are the only type of actuator available in a Lego Mindstorm kit,
642 a mechanism which converts rotational motions into a “grasping motion” is needed. In this
643 study, a rotational grasping design was chosen for the gripper and an attempt was made to
644 “upgrade” the gripper by equipping it with the capability to undo the connection between two
645 Lego Duplo blocks, using the exact same rotational grasping motion. In addition, rectangular
646 patches of Egrips material [42] were glued to the surface of the flat plate to improve the
647 coefficient of friction. An additional fixture was also added to the gripper to provide an
648 attachment point for the lift drive. The realization of the final design of the gripper is shown in
649 Figure 7(a).

650 Regarding the design of forward drive sub-module, the number of wheel types available
651 were limited to two: cylindrical wheels or caterpillar tracks. It is desirable to have as much
652 contact with the ground as possible to spread out the load. Since the forward drive module also
653 has to carry both the lift drive and the gripper module, the caterpillar tracks coupled with one
654 servo motor were thus chosen for our forward drive. Its realization is shown in Figure 7(b).

655 Given that the purpose of our lift drive is to enable vertical translation of the gripper, and
656 that the only type of actuator available in a Lego Mindstorm kit is servo motors, one needs to
657 design a mechanism which converts rotational motion into a linear motion. There are two main
658 types of design for lift drive: (1) The crank-slider design and (2) The scissors design. In this
659 study, it was found that the maximum vertical translation of the crank-slider design was
660 insufficient by taking into account the height of the 3D structure that needs to be built. For this
661 reason, the scissors design was chosen for our lift drive. The realization of the lift drive design
662 is shown in Figure 7(c).

Insert Figure 7 approximately here

663 Finally, the support structure comprises an elevated runway with runway guards, as shown
664 in the right side of Figure 3, with the stock and assembly space.

665 **4. Validation**

666 In this section, two tests were designed and conducted to demonstrate the feasibility of the
667 proposed RPS. In the tests, the hardware and software were connected wirelessly using
668 Bluetooth to make the RPS automated. The test models created were an N-by-N stack of single
669 Jenga blocks and two wall designs as shown in Figure 8.

Insert Figure 8 approximately here

670 The first test consisted of two different structures to (1) assemble WallDesign1 (Figure
671 8(a)), and then to (2) refabricate WallDesign1 into WallDesign2 (Figure 8(b)). The first half of
672 the test was completed successfully, with the occasional difficulty in connecting the top Lego
673 bricks firmly to the Lego door due to placement inaccuracy. For the second half of the test, a
674 correct refabrication sequence was computed, with two key emphases:

- 675 1. The system recognized that the three Lego blocks from WallDesign1 must be treated
676 as a single entity during the disassembly process, since the Lego's connectors are
677 assumed to be permanent connectors.
- 678 2. The system also recognized that even though WallDesign1 and WallDesign2 have both
679 the three Lego blocks and the Jenga blocks on the bottom right corner as common parts,
680 it must disassemble the Lego blocks so that the Jenga blocks on the bottom left corner
681 can be disassembled, and can only leave the bottom right corner as is.

682 The RPS computed correctly the disassembly sequence {1, 2, 3} of WallDesign1 and the
683 refabrication sequence {5, 2, 6} into WallDesign2 by taking into account the presence of the
684 permanent connectors and the common part numbered 4.

685 However, despite the correct refabrication sequence being computed, manual intervention
686 had to made to complete the second disassembly operation, in which the group of three Lego
687 blocks must be lifted over the group of 4 Jenga blocks on the bottom left corner, as the robot’s
688 maximum lift height was insufficient.

689 In the second test, the command to refabricate could come at any time during the
690 WallDesign1 assembly process. The system performed this test as successfully as the first test,
691 by keeping track of the assembly process and generating the correct refabrication sequence
692 regardless of what state the existing structure was in. A snapshot of the entire system after
693 having completed the final test is shown in Figure 9.

Insert Figure 9 approximately here

694

695 **5. Conclusion and future work**

696 With the aim of increasing the design flexibility of current prefabrication methods, a system
697 called RPS consisting of hardware and software modules was developed to demonstrate a new
698 concept called “refabrication”: the automatic disassembly of a prefabricated structure and its
699 reconstruction according to a new design.

700 Two key algorithms within the software module were developed in this study for
701 implementing the RPS. An algorithm was developed to automatically compare the old and new
702 3D models and identify all components which the two models do not have in common. Upon
703 testing, this algorithm identified the correct differences between two non-trivial 3D models. In
704 addition, an algorithm was developed to automatically compute the optimal refabrication
705 sequence that would transform one model into another when given the differences between the
706 two design models. This desired function was broken down into two sub-functions. First, the
707 number of (dis)assembly operations required for the removal of any one single subassembly

708 must be calculated. In order to achieve this, the algorithm incorporated a stripped-down version
709 of the NDBG technique. Second, the smallest number of (dis)assembly operations required for
710 the removal of all not-in-common subassemblies must be calculated. This was achieved by
711 comparing three different alignment scenarios for the two models, calculating the total number
712 of (dis)assembly operations required in each scenario, and finally picking the scenario with the
713 smallest number of operations required. Upon testing, this algorithm also calculated the correct
714 (dis)assembly sequence for the two 3D models mentioned with two notable successes: (1) The
715 connectors between Lego blocks were assumed to be permanent connectors, and the system
716 successfully recognized that connected blocks must therefore be treated as a single entity
717 during the disassembly process; (2) The system also recognized that certain components which
718 are common to both models must still be removed if such components are blocking the
719 disassembly path of not-in-common components.

720 A hardware system was developed to demonstrate the working of the developed algorithms
721 in real-time. This system performs all assembly operations with successful placement precision
722 although some disassembly operations needed manual intervention due to insufficient
723 maximum lift height. The scope of this study was, however, restricted to the refabrication of
724 assemblies which employ only stacking operations (1D) and subassemblies of cuboid shapes.
725 The results from this study could therefore be scaled-up and applied to a more realistic problem
726 set by incorporating the full version of the NDBG technique, which accounts for 2D assembly
727 operations and subassemblies of arbitrary polygons. Future investigations are warranted to
728 extend the applicability of the proposed system as follows:

- 729 - Incorporating stability analysis algorithm to the assembly sequencer
- 730 - Adding a motion planner to ensure assembly operations are executed in optimal time
- 731 - Taking into account arbitrary placement of connectors as additional constraints on the
- 732 assembly sequencing process

733 - Incorporating computer vision techniques to achieve better placement precision for the
734 gripper arm

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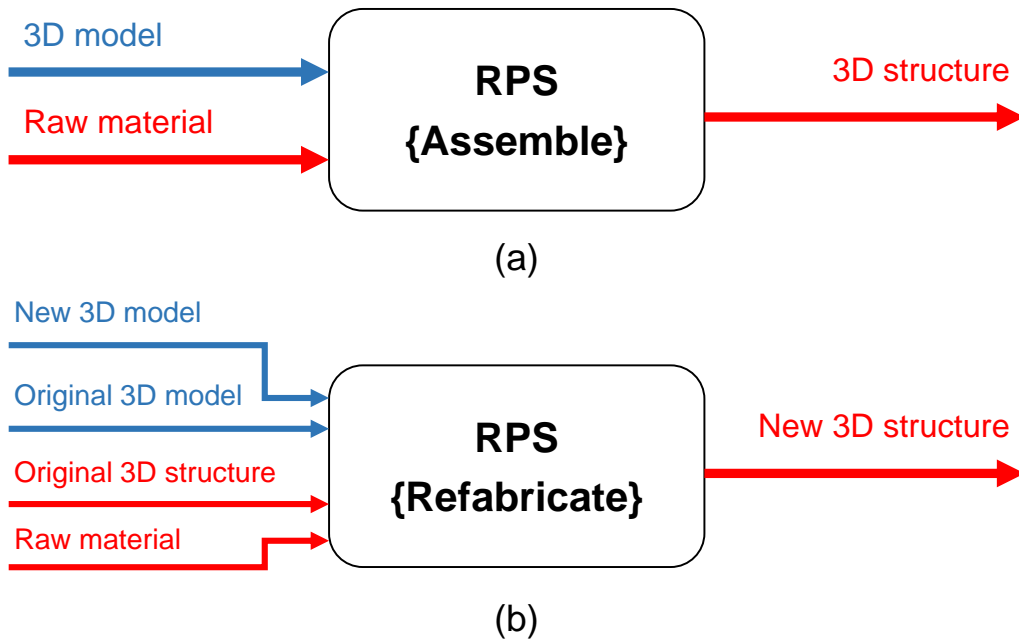
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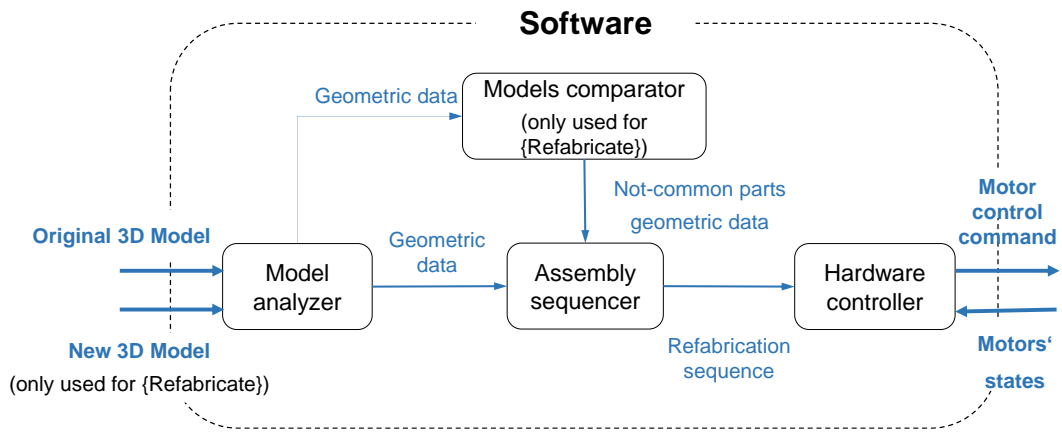
Figure 1. The two functions of RPS: (a) Assemble and (b) Refabricate

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*Note: The blue and red arrows represent digital and physical quantities, respectively.

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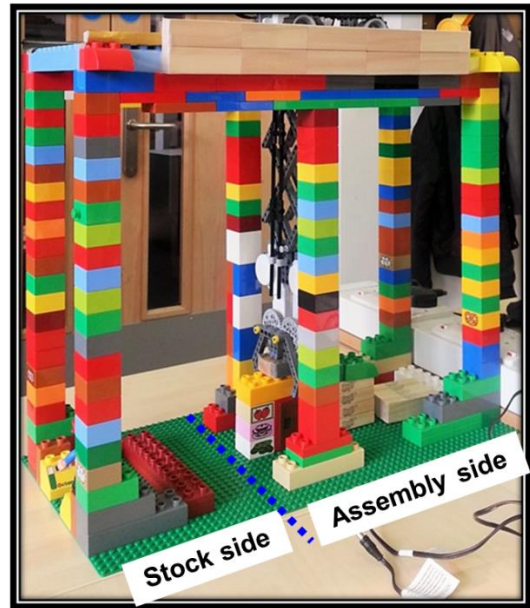
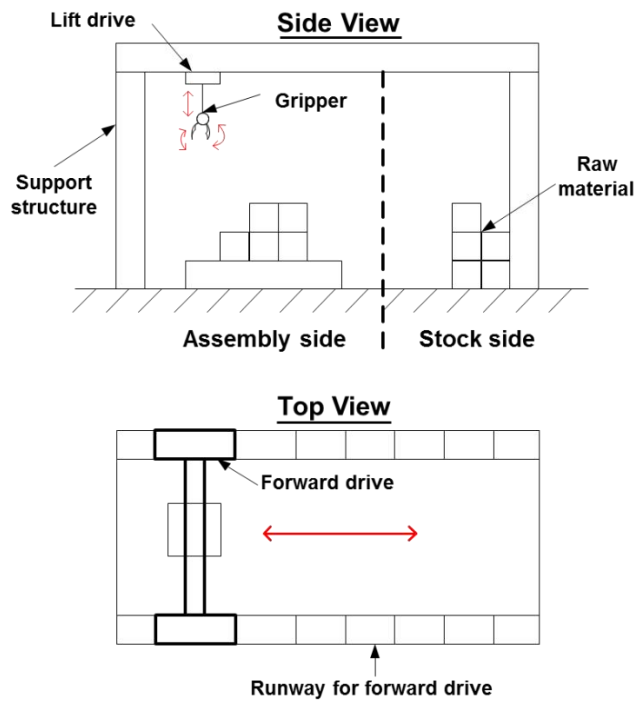
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Figure 2. Design of the RPS software module

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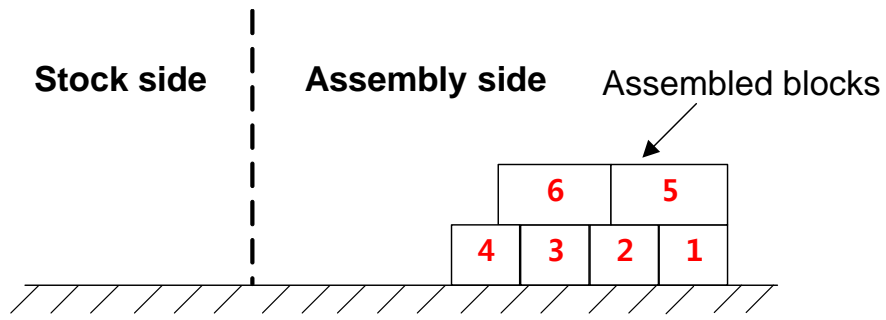


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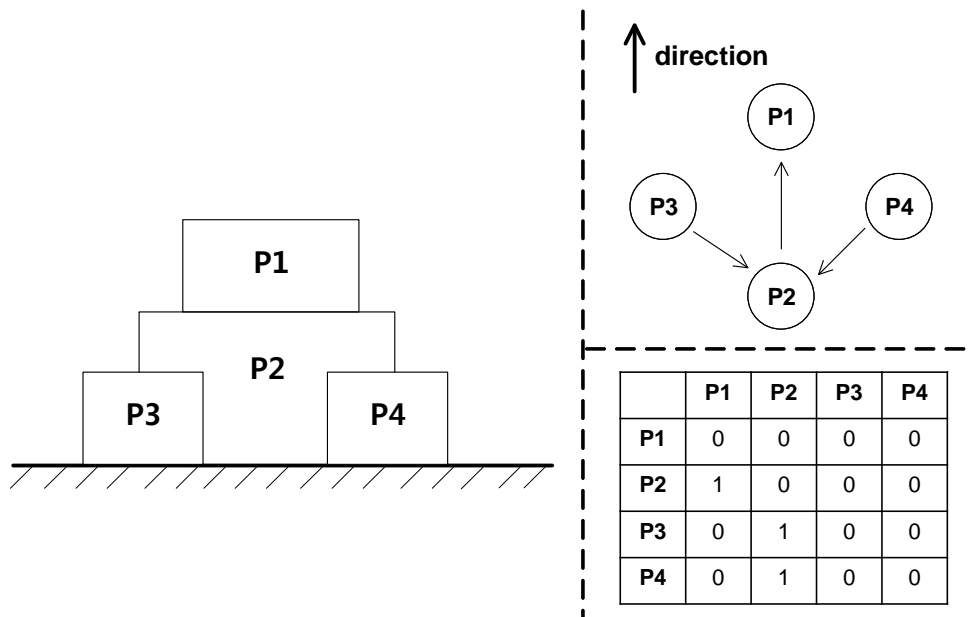
Figure 3. Design of the RPS hardware module

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Figure 4. An example assembly sequence calculated by the assembly sequencer

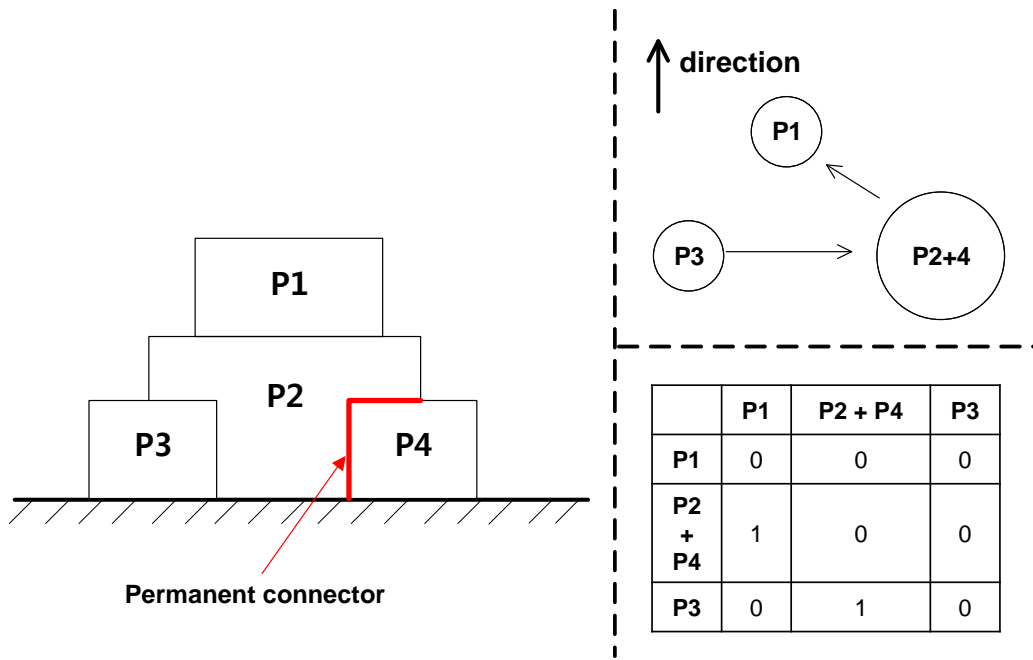


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Figure 5. Example of a DBG & its matrix representation

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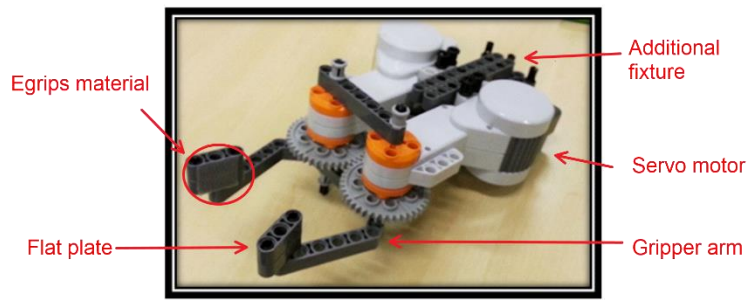


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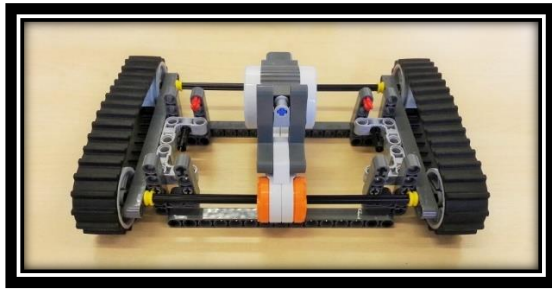
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Figure 6. Example of a truncated DBG & its matrix representation

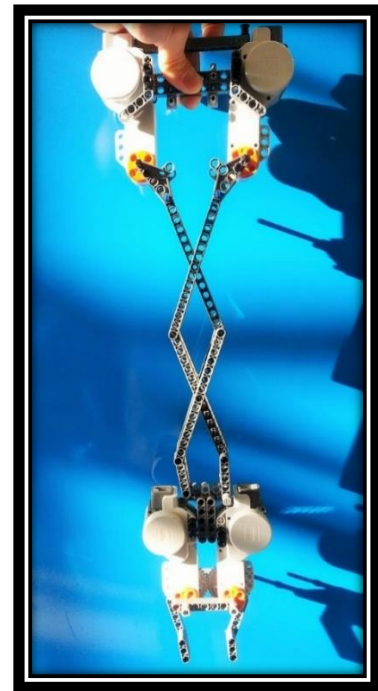
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(a) Gripper



(c) Forward drive

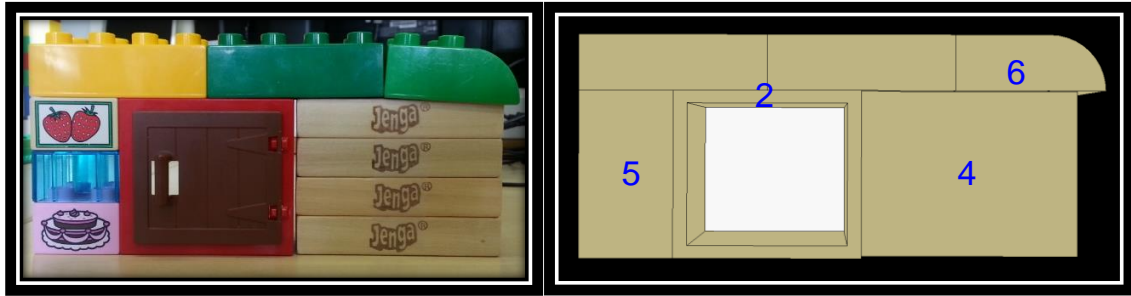


(b) Lift drive (coupled with the "gripper" sub-module)

Figure 7. Hardware submodules: (a) gripper, (b) lift drive, and (c) forward drive.



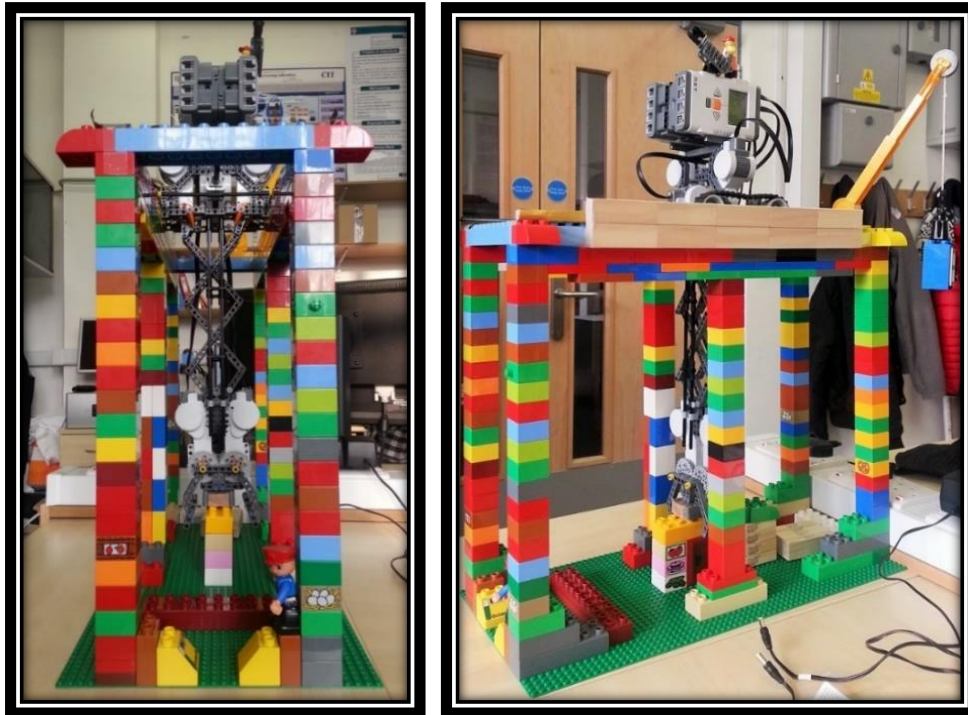
(a)



(b)

892 **Figure 8.** Real-life and digital versions of test model: (a) WallDesign1 and (b) WallDesign2

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Figure 9. Snap-shot of the entire system after completing the final test