

1 Towards Enduring Autonomous Robots via Embodied Energy

2
3 Cameron A. Aubin,^{a*} Benjamin Gorissen,^{b,c} Edoardo Milana,^c Philip R. Buskohl,^d Nathan
4 Lazarus,^e Geoffrey A. Slipper,^f Christoph Keplinger,^g Joshua Bongard,^h Fumiya Iida,ⁱ Jennifer A.
5 Lewis,^{b*} Robert F. Shepherd,^{a*}

6
7 *Authors contributed equally to the concept and writing of this manuscript

8
9 ^aCornell University, Mechanical & Aerospace Engineering. ^bHarvard University, School of Engineering & Applied
10 Sciences. ^cKU Leuven, Production Engineering. ^dAir Force Research Laboratory, Materials and Manufacturing
11 Directorate. ^eArmy Research Laboratory, Energy and Biotechnology Division. ^fArmy Research Laboratory,
12 Autonomous Systems Division. ^gMax Planck Institute for Intelligent Systems, Robotic Materials Department.
13 ^hUniversity of Vermont, Computer Science. ⁱUniversity of Cambridge, Department of Engineering.

14 15 Preface:

16
17 Autonomous robots are comprised of actuation, energy, sensory, and control systems built from
18 materials and structures that are not necessarily designed and integrated for multifunctionality.
19 Yet, animals and other organisms that robots strive to emulate contain highly sophisticated and
20 interconnected systems at all organizational levels, which allow multiple functions to be performed
21 simultaneously. Herein, we examine how system integration and multifunctionality in nature
22 inspires a new paradigm for autonomous robots that we call *Embodied Energy*. Currently, most
23 untethered robots use batteries to store energy and power their operation. To extend operating
24 times, additional battery blocks and supporting structures must be added, which increases weight
25 and reduces efficiency. Recent advancements in energy storage techniques enable chemical or
26 electrical energy sources to be embodied directly within the structures, materials, and mechanical
27 systems used to create robots. This perspective highlights emerging examples of Embodied
28 Energy, focusing on the design and fabrication principles of enduring autonomous robots.

29 30 31 Manuscript Body:

32 33 Embodied Energy: a new paradigm for robotics

34
35 Power and control remain major barriers to the realization of untethered autonomous robots that
36 can move and adapt on demand for long duration missions. A close synergy between active
37 systems is needed to optimally use the, often limited, onboard energy supply. Recent examples
38 highlight a pathway towards improved operational lifetimes through the co-integration of chemical
39 and electrical energy sources with mechanical systems to imbue robots with high energy and power
40 density¹⁻⁵. By housing the energy supply directly within the robot's architecture and materials, it
41 is readily available for use, can be efficiently converted into useful work and, ideally, can be
42 replenished through onboard energy harvesting mechanisms. We call this design philosophy
43 *Embodied Energy*, where the same mass that normally provides a vital mechanical or structural
44 function also contains stored energy that powers at least a portion of the robot or device.

45
46 The potential of Embodied Energy systems can be evaluated through biological analogy. In
47 humans and other animals, energy is primarily stored in the body as fat. However, the
48 functionalities of adipose tissue extend far beyond energy storage to include insulation, the

49 protection of vital organs, waterproofing, and the regulation and production of hormones.
50 Embodied Energy can similarly imbue robotic systems with multifunctionality. For example,
51 batteries can be configured to serve load-bearing or architectural functions. Compliant materials
52 and actuators can provide structure while storing and reusing elastic energy.

53
54 In many ways the underlying principles of Embodied Energy parallel those currently employed in
55 robotic artificial intelligence systems. AI-driven robots interact with their environment based on
56 information previously gathered and processed from their surroundings via onboard sensors. This
57 closed sense-decide-response loop is reliant on a continuous synergy between the sensors,
58 processors, actuators, and collected data. The same should be true for the energy harvesting-
59 storage-delivery loop in robots with Embodied Energy. If these systems can fulfill energy and
60 power needs as well as actuation and control functions, we can create robots that more seamlessly
61 interface with their own environments.

62
63 Over the past two decades, there has been a small, but growing, effort to improve machine
64 autonomy by developing multifunctional, Embodied Energy systems^{4,5}. Most robots, however, still
65 contain isolated power, actuation, sensory, and control *blocks*, each optimized for an individual
66 task (Fig. 1)^{1,3,6-8}. In Honda's ASIMO robot, for example, there is a clear division between the
67 actuators in the joints, the control module in the torso, and the batteries in the backpack unit⁶. Such
68 isolated building blocks lack the synergy and efficiency observed in living organisms (e.g., the
69 pictured octopus), which are capable of harvesting, storing, and generating energy either
70 continuously or on demand. By distributing energy sources throughout multifunctional system
71 configurations, as illustrated by the progression of innovative robots and their corresponding block
72 diagrams in Fig. 1, we can expand their range of complex functions while increasing their
73 operational efficiency.

74 75 **Energy storage and conversion**

76
77 An important aspect of Embodied Energy design is precisely how this energy is harvested, stored,
78 applied, and recovered throughout the robotic system. Most untethered robot designs are guided
79 by a simple tradeoff between size, weight, and power. However, by broadening the range of
80 functionalities concurrent in a material or subsystem and distributing the mass budgets between
81 them, we can upend the conventional energy budget and design methodology. Power, sensing,
82 computation, and control will be largely native to the mechanical system.

83
84 Fig. 2 details concepts that are important to consider when designing for Embodied Energy.
85 Several robotic Embodied Energy systems, each representing a specific energy storage and
86 transduction methodology, are exemplified here. Though energy storage can take many forms in
87 mechanical systems, we limit our depiction here to five of the most common types that can be
88 harnessed by autonomous robots: electrical, mechanical, chemical, magnetic, and thermal. Several
89 of these categories overlap in conventional systems (e.g., electrochemical batteries,
90 thermochemical heat storage), a property that can be leveraged when merging different energy
91 storage and transduction technologies. Systems that store energy can vary wildly in their efficiency
92 (see Extended Data Table 1), material composition, and even the states of matter they interface
93 with (e.g., solid state batteries, liquid redox flow batteries, and gaseous hydrogen fuel cells).
94 Similarly, the landscape of energy transduction mechanisms (e.g., electromagnetic motors,
95 combustion engines, hydraulic pistons, etc.) is vast, complicating design decision making.

96

97 The intersection of energy storage and transduction will form the framework of our discussion, as
98 Embodied Energy seeks to accomplish these tasks collectively. Generally speaking, Embodied
99 Energy is best discussed in the context of robotics by examining its conversion to mechanical work
100 (i.e., actuation and locomotion). In the sections that follow, we will present existing technologies
101 that can transduce different types of stored energy into mechanical actuation in robots. We will
102 describe how these technologies can be implemented in multifunctional Embodied Energy
103 systems, citing existing examples, and discuss future developments for each energy transduction
104 category, concluding with an examination of nine Embodied Energy design principles.

105

106 *1. Electrical to mechanical transduction:*

107

108 Untethered robots and their mechanical actuators are predominantly powered by rigid rechargeable
109 batteries (e.g., lithium-ion, lithium-polymer, nickel-metal hydride, etc.). Some of the earliest
110 notable cases of multifunctional energy storage involve structural power sources^{5,9,10}, where static,
111 load-bearing components of machinery also supply electrical energy. A simple example is the use
112 of lead-acid batteries in forklifts as counterbalance for lifting heavy loads¹¹. More sophisticated
113 Embodied Energy examples include structural batteries in satellites¹², spacecraft¹³ and electric
114 vehicles^{4,14}, lithium-polymer batteries that function as wings in unmanned aerial vehicles
115 (UAVs)⁹, pliable, biomorphic zinc-air batteries that can serve as protective covers for robots¹⁵, and
116 flexible galvanic thin-film batteries in flapping wing aerial vehicles (FWAVs)¹⁶. In the latter
117 example, the use of embodied electrical energy sources increased the operating time of an FWAV
118 by 250% relative to designs using standard batteries and conventional wing materials.

119

120 The conversion of electrical energy to mechanical actuation is most commonly accomplished in
121 robots by electric motors, though they do not store their own onboard energy. Electroactive
122 polymers (EAPs), so-called because they change size or shape in response to electric stimulus, are
123 a class of materials that are capable of multifunctional energy storage. They have the capacity to
124 quickly ($t \sim 10^{-3}$ – 10^{-4} s) undergo large reversible strains ($\epsilon_{ult} > 300\%$)^{17,18} making them an attractive
125 option for robots with muscle-like actuators^{17–19} and sensing capabilities^{20,21}. EAPs can broadly be
126 classified as either electronic (e.g., electrostatic, electrostrictive, and ferroelectric polymers) or
127 ionic (e.g., gels and ionic polymer-based composites) depending on their mode of action¹⁸.

128

129 Dielectric elastomer actuators (DEAs), a class of soft electrostatic transducers belonging to the
130 electronic group, have been performing multifunctional electrical to mechanical energy conversion
131 for decades²². During operation, DEAs store energy throughout their structure, with elastomer
132 layers functioning as deformable capacitors. Consequently, DEAs can serve simultaneously as
133 actuators, sensors, and energy harvesters²³. DEAs have been implemented in crawling^{24,25},
134 gripping²⁶, swimming^{27–29}, and even flying robots³⁰, while more recently introduced soft
135 electrostatic transducers (e.g., hydraulically amplified self-healing electrostatic (HASEL)
136 actuators^{31,32}) have combined solid and liquid dielectrics to produce additional functionalities,
137 including hydraulic and pneumatic³³ actuation modes. Unlike conventional electric motors, soft
138 electrostatic transducers inherently store electrical energy and can assume “catch states”, where
139 negligible power is consumed while holding a position. When used in a multifunctional manner,
140 soft electrostatic transducers provide a rich opportunity for Embodied Energy in robots, and have
141 already been used for high frequency, high amplitude actuators^{32,34,35}

142

143 Ionic polymer-metal composites (IPMCs) have also been used in the creation of mobile robots^{36–}
144 ³⁸. Composed of a thin conductive polymeric material placed between two metal electrodes, IPMCs
145 use the transport of ions into and out of the polymer for actuation. Though they generally produce
146 lower actuation forces compared to soft electrostatic transducers, their ability to operate at low
147 voltage ($V_{in} \sim 1\text{-}5\text{ V}$, vs $V_{in} > 100\text{ V}$ for DEAs) and also generate a small voltage in response to
148 deformation has made IPMCs both useful actuators and sensors in biomedical and engineering
149 applications^{21,39–41}.

150
151 We anticipate future improvements not just in the energy density of batteries, but also in the
152 materials used in their composition⁴². Batteries with tunable mechanical properties could serve a
153 variety of functions outside of traditional energy storage, expanding the benefits of Embodied
154 Energy to a wider array of robot designs. As exemplified in Fig. 2, a stretchable battery can
155 theoretically be used as an extensible tendon in a walking robot or a wearable exosuit, thus
156 combining electrical and elastic energy storage into a structural element that connects different
157 system components. Fluidic energy storage using flow battery technologies is also a key
158 innovation in this domain. For example, in 2019, a soft robotic fish was created with an embedded
159 “electrolytic vascular system¹.” This design was inspired by redox flow batteries and consisted of
160 a distributed liquid electrolyte that also served as a hydraulic fluid. This multifunctional use of
161 electrochemical energy storage enabled simultaneous power generation and fluidic actuation,
162 which allowed the fish to swim for long durations (>36 h).

163 164 2. Mechanical to mechanical transduction: 165

166 There are many methods for converting stored mechanical energy into motion, including springs,
167 linkages, gear trains, cams and followers, etc. However, multifunctional and embodied
168 applications are far less common in modern machinery. One use case that has been explored is the
169 inclusion of flywheels in spacecraft to both store energy and provide torque for attitude and
170 control^{43–45}.

171
172 For robots, one pathway towards improved mechanical energy management involves
173 advancements in high energy density materials, composites, and interfacial chemistry that can
174 replace or supplement existing mechanisms. The field of soft robotics has provided such a platform
175 for the latest innovations in Embodied Energy due to the vast design space offered by the high
176 strain capabilities ($\epsilon_{ult} > 1,000\%$), range of stiffnesses ($E \approx 1 - 10^5\text{ kPa}$), and durability of soft
177 matter, such as silicone elastomers, hydrogels, and polyurethane rubbers⁴⁶. Other characteristics
178 of soft robots, including their ability to be fabricated via additive manufacturing methods (e.g., 3D
179 printing and soft lithography)⁴⁷, the existence of well-established actuation techniques (e.g.,
180 fluidic, electrostatic)^{46–48}, adaptability, and human compatibility, all motivate synergistic
181 applications for multifunctional and efficient power conversion technologies.

182
183 Soft robotics has historically embraced the storage or tuning of elastic energy in elastomeric
184 structures for improved efficiencies and high-power actuation. Recent work has pushed this further
185 by harnessing materials and geometric nonlinearities to discretize the actuator response. Some
186 nonlinear soft actuators, for example, are characterized by instabilities that cause the actuator to
187 undergo a snap-through response, where a fast motion with a large stroke follows from a small
188 external input. During the snapping phase, the elastic energy stored in the actuator structure is
189 suddenly released and can be redirected towards the external world. This principle was recently

190 exploited in the fabrication of bistable hybrid soft actuators inspired by the spinal flexion of
191 mammalian quadrupeds⁴⁹. In another example, stored pressure-volume mechanical work was
192 harnessed to create a jumping robot consisting of spherical caps that leveraged a volumetric
193 instability⁵⁰. Embedded actuator sequencing has been achieved by connecting multiple nonlinear
194 balloon actuators, adding passive control to the energy conversion process^{8,51}. We see this snap-
195 through behavior in nature as well; a classic example is that of the venus flytrap⁵².

196
197 As robots continue to emulate biology and evolve towards hybrid hard-soft structures, there will
198 be additional opportunities to generate unified musculoskeletal systems that provide energy
199 storage, power, and structural functionality. Series elastic actuators (SEA), where a spring-like
200 element is placed between an actuator and the end effector, is perhaps the simplest example of this
201 concept. Fig. 2 highlights how this approach to Embodied Energy can be used to improve the
202 adaptability and durability of terrestrial robots. Integrating compliant elements like SEAs into
203 robot architectures could lead to greater shock tolerance, more accurate and stable force control,
204 lower reflected inertia, and decrease inadvertent damage to the environment, all while storing
205 energy⁵³. Advancements in manufacturing techniques will also inform future designs for hybrid
206 hard-soft robots that can structurally store mechanical energy. Multi-material additive
207 manufacturing represents a clear step towards this approach. An idealized process would be able
208 to dynamically tune the chemical and mechanical properties of a part during synthesis to produce
209 functionally graded composites and monolithic robots. Just as humans capture and reuse elastic
210 energy with their muscles and tendons, we also expect future robots to more commonly harvest,
211 store, and reuse energy from inertial forces⁵⁴.

212 3. *Chemical to mechanical transduction:*

213
214 Humans and other animals rely on chemical fuels like glucose and fat to serve as their primary
215 energy source for mechanical work. Similarly, combustion engines convert energy-dense
216 hydrocarbons into power for transportation, but the high temperatures required necessitate the use
217 of rigid and dense metal bodies (or frameworks) in most applications. Compressed, gaseous
218 hydrocarbon fuels have now been used for both variable compliance⁵⁵, as well as, when
219 combusted, high power density actuation in soft elastomeric robots². While the efficiency is not
220 yet high, the large energy density of these hydrocarbon fuels, along with their multifunctional
221 capabilities, can increase the high power performance and adaptability of these robots compared
222 to inert gases^{55,56}. More recently, liquid fuels have been implemented in multifunctional power-
223 structure-actuation systems to achieve cyclic movement in untethered robots⁵⁷. The “octobot”,
224 unveiled in 2016, employed a distributed chemical energy system (platinum-catalyzed H₂O₂
225 decomposition) coupled with a microfluidic logic circuit to autonomously achieve mechanical
226 actuation of the tentacles of a 3D printed octopus³.

227
228
229 We anticipate further advances by storing convertible fuel sources within intelligent structural and
230 machine elements. Autophagous systems are one such approach, wherein physical loads are borne
231 by structural components that also provide energy in a “self-consuming” process. Prior work in
232 this area has been explored for use in aerospace applications^{5,58}. The structural requirements for
233 launching vehicles into space greatly exceed those needed for normal operation; with the
234 components consequently sized for launch, the lifetime and efficiency of these vehicles would
235 increase by breaking down and harvesting energy from their excess materials. This same strategy
236 could be implemented in robots, and is supported by research involving autophagous metal-air

237 batteries⁵⁹, structural beams pressurized with gaseous fuels⁵⁸, and thermoplastic matrix composites
238 that can be converted to fuel and burned with liquid oxidizers⁶⁰.

239
240 Naturally, end-use applications must be carefully considered when designing autophagous
241 structure-power systems. The large energy density of solid fuels comes at the expense of ease-of-
242 servicing and long-term durability as the structure is depleted. Recyclable, biodegradable, and
243 single-use devices do show promise in applications including surveillance, exploration, and
244 medicine, but more traditional robots will need to prioritize refueling capabilities, possibly through
245 the use of modular designs, energy harvesting, and secondary or emergency means of power
246 generation to ensure perpetual functionality. One difficult challenge that can be envisioned is the
247 nonhomogeneous consumption of materials in autophagous systems. Using the autophagous
248 metal-air battery as an example, a localized catastrophic failure could incapacitate the system,
249 leaving a fraction of the remaining energy inaccessible. A solution to this problem is the use of
250 materials and configurations that leave behind residual structures that can still function in their
251 intended roles. Bimetallic shells could be used in configurations where only one of the two
252 compounds is consumed. Porous structures containing internalized liquid or adsorbed gaseous
253 fuels are another promising solution, as shown in Fig 2. A recent report described an ultraporous
254 ($7,310 \text{ m}^2 \text{ g}^{-1}$) metal-organic framework that can store large volumes of methane and hydrogen
255 gases that could be used to power vehicles, aircraft, and even robots⁶¹.

256 257 4. Magnetic to mechanical transduction: 258

259 The coupling of electricity and magnetism leads to a fair degree of overlap when discussing
260 magnetic energy storage applications. Energy can be stored in the magnetic field of an inductor or
261 a superconducting coil (a process called superconducting magnetic energy storage, or SMES), for
262 example, but current flow is required. Many robotic components and actuators, including motors,
263 valves, pumps, solenoids, switches, and relays all leverage this same basic electromagnetic
264 principle: a conducting coil produces a magnetic field when energized by an electric current, which
265 in turn induces movement in a magnetic body.

266
267 Many improvements to magnetic actuators have been realized over the past few decades, most
268 recently with regard to smaller size scales and the adoption of different substrate materials⁶²⁻⁶⁵.
269 Magnetic microrobots, in which the body and magnet are mostly one and the same, represent an
270 exciting new set of capabilities, especially in the biomedical or *in vivo* realms⁶⁶⁻⁶⁸. Constructing
271 the robot from magnetic materials allows the transduction of magnetic energy into mechanical
272 motion to be embodied at the structural level. While remote power generation eliminates the need
273 for an integrated energy storage system, external control via bulky, stationary magnetic coils
274 restricts the scope of these robots to some degree.

275
276 Though examples are limited, magnetic actuation presents an excellent opportunity for Embodied
277 Energy technologies, as the coil and magnet configurations used for actuation can also be used for
278 energy harvesting (a magnet traveling through a coil will induce an electromotive force, while
279 electrically powered actuators can in turn move magnetic elements). One example is the use of
280 electromagnetic dampers^{54,69} within end effectors for proprioceptive force control, energy
281 generation, and locomotion, as demonstrated in Figure 2. Another example is the “Moball” robot,
282 which contains moveable, permanent magnets that can provide steering and enable rolling
283 movements by changing the device’s center of mass, in addition to generating energy by passively

284 oscillating within solenoids⁷⁰. Magnetic actuator technologies are also being expanded to non-rigid
285 materials; stretchable inductors for compliant power electronics^{71,72} are one interesting emerging
286 application.

287
288 Improvements in offboard magnetic control will be required for future robots to maximize the
289 potential of Embodied Energy in this domain. We can also envision coupling magnetic actuation
290 and energy harvesting/delivery with the existing electrical systems in larger robots to achieve
291 higher efficiencies and a wider range of functionalities.

292
293 *5. Thermal to Mechanical transduction:*
294

295 Thermal to mechanical energy conversion is commonly accomplished by combustion engines,
296 which are ubiquitous in modern machinery. However, the mechanical complexity, weight, size,
297 and scaling limitations of heat engines complicate integration into other energy-power systems
298 and typically restrict them to larger applications in industry and transportation. Heat engines make
299 up for their lower efficiencies (efficiency $\eta \sim 25\text{--}40\%$)⁷³ relative to other energy transducers by
300 consuming high energy density reactants. One established technique for improving the efficiency
301 and expanding the utility of combustion engines is the capture and reuse of waste heat (e.g.,
302 through the use of exhaust gas heat recovery, organic Rankine cycle units, or thermoelectric
303 devices)^{73,74}. Another approach is to leverage an alternative fuel source shared by another onboard,
304 power-generating device. Hybrid electric vehicles represent a simple example where an electric
305 and thermal system can operate synergistically through the addition of an optimizing control
306 element. A related technology is combined heat and power (CHP), wherein fuel is used in the
307 concurrent production of electricity and thermal energy, the latter of which is efficiency captured
308 and used in processes like heating and cooling. The energy systems of future robots could all stand
309 to benefit through the incorporation of similar processes.

310
311 At smaller size scales, bimetallic strips are among the simplest technologies used for thermal
312 actuation. Heating a pair of thin, bonded metal parts with different coefficients of thermal
313 expansion will cause the strip to bend. Recently, this technique of coupling materials with different
314 thermal properties has been extended to soft matter to create fiber-based, muscle-like actuators
315 capable of producing large stroke cycles and withstanding high strain (in some cases $>1,000\%$)^{75,76}.

316
317 Thermophoresis, a phenomenon where temperature gradients cause particles to experience a net
318 force that may induce flow, represents another instance of thermal to mechanical energy
319 transduction. Over the past few decades there has been growing interest in using thermal gradients
320 to manipulate and propel micro/nano scale objects. Recent achievements in the medical field
321 include the creation of thermophoretic nanomotors that can target and penetrate cancer cells⁷⁷, and
322 the development of a micro-rocket robot that can be optically actuated through a bloodstream⁷⁸.

323
324 Shape memory polymers (SMPs) are another promising class of materials/actuators that can be
325 engineered to react to both thermal and magnetic stimuli. As their name suggests, SMPs are
326 capable of undergoing a shape transformation—the entropy-driven restoration of a prior
327 mechanical deformation—that is fast, reversible ($t_{\text{recovery}} < 1$ sec to minutes), and
328 reprogrammable⁷⁹. The favorable mechanical properties of SMPs, including high ultimate strains
329 ($\epsilon_{\text{ult}} < 800\%$), tunable stiffnesses ($E = 10^4\text{--}3$ GPa), and a wide range of transition temperatures
330 ($T_{\text{crit}} = -10\text{--}100$ °C)⁸⁰ have seen them used in medical devices^{81,82}, fabrics and wearables⁸³,

331 sensors⁸⁴, robots^{85,86}, and aerospace technologies⁸⁷. Additionally, the multifunctionality associated
332 with storing several different shape configurations within a single or composite material^{79,88,89},
333 which can serve as both a structure and an actuator⁸⁶, makes SMPs an attractive option for
334 Embodied Energy technologies. Shape memory alloys (SMAs) comprise a similar group of smart
335 materials that can return to their original forms when subjected to changes in temperature or
336 magnetic field strength. SMAs are typically stiffer than SMPs ($E \sim 28\text{--}83$ GPa, with generally
337 similar moments of inertia)⁸⁰ and while they possess limited strain capabilities ($\epsilon_{ult} < 8\%$)⁹⁰ their
338 high power densities ($\Gamma = 10^3\text{--}10^5$ kW m⁻³)⁴⁸ have contributed to their use in a wide array of robots
339 and actuators⁹⁰⁻⁹⁵.

340
341 With waste heat being a significant byproduct of many mechanical systems, it is easy to visualize
342 how SMAs and SMPs could be integrated and embodied within existing machine architectures to
343 improve energy efficiency, weight, or device performance. Both materials, for example, could be
344 used as structural or skin-like elements that actuate to allow thermoregulation in different
345 machines. Shape memory actuators could also be configured to respond to the waste heat of solar
346 energy harvesters or heat engines, or used in concert with thermoelectric or pyroelectric
347 devices^{96,97} (Fig. 2). A recent report detailed the creation of an insect-scale, autonomous crawling
348 robot containing a platinum-coated SMA artificial muscle that was powered via catalytic
349 combustion with an onboard methanol fuel supply⁹⁸. Another publication demonstrated how low-
350 grade waste thermal energy could be converted into electrical energy through the use of artificial
351 polymer muscles.⁹⁹ More than 120 W of electrical energy per kilogram of muscle were
352 successfully produced, which could be used in powering autonomous sensors.

353

354 *Embodied Energy design principles:*

355

356 Creating robots that effectively embody energy can be accomplished by optimizing for endurance
357 and operating time, while overcoming key design contradictions (e.g., increasing the energy
358 content of a robot while maintaining its volume.). To that end, we have identified several key
359 design principles that can be applied during robot development and production. Fig. 2 depicts how
360 these design principles can be used in both existing and hypothetical Embodied Energy
361 technologies.

362

363 1. *Design with size, weight, and power tradeoffs in mind.* While power density is inversely
364 proportional to weight and volume, operating time scales proportionally with size in
365 untethered robots. Using embedded, energy dense fuels is one approach to optimizing for
366 high power at smaller sizes. The prospect of integrated versus modular assembly represents
367 another aspect of this tradeoff. Modular designs can be easier to assemble, service, and
368 reuse. A complex and heavily integrated design can likely achieve higher performance and
369 should execute an array of self-sustaining functions, at the cost of simplicity in
370 maintenance.

371

372 2. *Integrate energy storage into structural elements.* Using batteries as structural elements
373 can eliminate the need for certain load bearing components. Mass or volume elements that
374 would normally bear loads can be reassigned to perform functions unrelated to energy
375 storage.

376

- 377
378
379
380
381
382
383
384
385
386
387
388
389
390
391
392
393
394
395
396
397
398
399
400
401
402
403
404
405
406
407
408
409
410
411
412
413
3. *Make a system serve itself by performing auxiliary helpful functions.* Synergistic systems can improve machine autonomy while limiting the need for human intervention. Halogen lamps represent a simple example—they regenerate their own filament when in use through the redeposition of evaporated metal¹⁰⁰. Similarly, in the RFB-inspired electrolytic vascular system¹ the same liquid used for hydraulic actuation is also used for energy storage, and the pumping of this liquid recirculates the soluble ions to improve the rate of charge transfer.
 4. *Use hybrid hard-soft structures to create adaptable designs.* Using compliant, muscle-like materials can lead to durable robots that can dampen or even absorb and redistribute forces, traverse difficult terrains, and operate with many degrees of freedom.
 5. *Use composite or porous materials to store energy.* Composites can contain both structural and energy storing domains. Similarly, porous materials, as in the example of gas adsorbent metal lattices⁶¹, can form lightweight structures that house fuel or energy in their pores.
 6. *Harvest energy from the environment.* To achieve fully autonomous robots, we must equip them with the technology to extract energy from their surroundings. Motion-driven microgenerators and photovoltaic cells are among the most mature energy harvesting technologies¹⁰¹, though efficiency and power density limitations exist (see Supplementary Information for a discussion of energy harvesting).
 7. *Reuse waste energy.* Recovered energy can be reconverted into onboard power, as in exhaust gas heat recovery systems, or repurposed for a secondary function, such as heating and cooling in CHP systems.
 8. *Leverage resonance.* Robot efficiency and longevity can be increased by driving systems with parameters that lead to high amplitude outputs. Further, operating actuators at resonance will require less energy input (e.g., a pneumatically powered actuator may need to be inflated fewer times and endure less stress for an equivalent distance traversed).
 9. *Compensate for weight through interaction with the environment.* Machine morphology should be adapted to derive advantages from their surroundings. Hydrofoils are used to lift ships out of the water to reduce drag, and vortex strips are implemented in aircraft wing designs to improve lift¹⁰⁰. In nature, many aquatic animals achieve buoyancy due to their energy storing fat reserves.

Challenges and future advancements

414
415
416
417
418
419
420
421
422
423

A universal methodology for characterizing and evaluating Embodied Energy systems in a design context has yet to be established. However, techniques for characterizing the advantages of multifunctional systems, in general, have been proposed. Johannisson et al. introduced a “residual performance methodology,” that involves comparing the specific properties (e.g., mass, shear strength, specific energy) of a multifunctional block with those of two or more monofunctional systems (e.g., structure, energy storage)¹⁰². Other approaches include establishing a multifunctional efficiency metric or directly calculating the change in a value of interest as a function of different design variables, though this relationship may not always be known. Thomas

424 et al. demonstrated this by modeling the flight endurance time of a hypothetical, electrically
425 powered UAV in terms of the relative masses of the onboard batteries, solar cells, and structure to
426 draw conclusions about the most effective multifunctional configurations⁵⁸.

427
428 To envision the potential efficacy of integrated energy storage and transduction systems, we
429 developed a multifunctional version of the classic Ragone plot¹⁰³, as shown in Fig 3. This graph
430 predicts the range of energy and power density values attainable by a theoretical, merged energy
431 storage and actuator system, based on the energy density, power density, and efficiency of the
432 component parts^{4,9,48,104–126} (see Fig. 3 legend for details). It is intended as a tool for exploring
433 different robot designs when energy and power requirements are known.

434
435 The pairs shown in Fig. 3 were selected based on complementary features or their usage in
436 previously reported prototypes (see Extended Data Table 1 for plotted values and their
437 corresponding references). The energy sources in these hypothetical combinations can be thought
438 of as fully embodied within their assigned energy transducer, where they will serve multiple
439 functions. Combinations 1–6, for example, can be thought of as structural battery configurations
440 used in concert with different electromechanical actuators. Combination 13 implies an engine or
441 turbine configuration that takes energy from the burning of its hydrocarbon support structure,
442 rather than a traditional fuel reservoir that serves a single energy storage function.

443
444 While the full scope of possible systems and combinations is impossible to sample, this data does
445 allow for a rough comparison of the energy content and output of different hypothetical Embodied
446 Energy arrangements. For example, combinations 10, 11, and 13 store energy as a hydrocarbon
447 fuel and are akin to autophagous power systems; however, despite possessing much greater energy
448 densities than many of the other systems, the upper bound of their power density range is not
449 significantly different from several battery and motor driven designs due to the low efficiencies
450 involved. The graph does not take into account mass budgets and efficiency penalties of
451 supplementary systems that may be necessary for the construction or operation of these
452 hypothetical systems. Similarly, this plot does not capture the additional functionalities or non-
453 energy storage characteristics that may be beneficial in certain designs (e.g., material
454 compatibility, scalability, or cost). All Embodied Energy technologies, along with their inherent
455 characteristics and design tradeoffs, must necessarily be evaluated in the context of their intended
456 environment and applications.

457
458 Embodied Energy both presents and promises to solve future challenges. Size, weight, and power
459 tradeoffs, for example, will always present difficulties to robotics researchers, particularly as
460 smaller robots and personal devices, each possessing significant payload restrictions and energy
461 requirements, are pursued. Microrobots present an extreme case, with many of the latest innovative
462 designs requiring an electric tether to deliver power¹²⁷. Several are limited to specialized
463 environments,¹²⁷ and most also forego conventional actuators (i.e., DC motors) due to fabrication
464 limitations as well as the unfavorable scaling of friction and electromagnetic forces¹²⁸. If the
465 advantages promised by microrobot technologies (e.g., swarm capabilities, exploration, search and
466 rescue, medical intervention) are to be realized, multifunctional design strategies employing
467 Embodied Energy must be pursued.

468

469 Other challenges must be overcome as well, including the need for new, compatible materials that
470 operate synergistically with existing technologies, as well as yet unimagined ones. Examples
471 include conductive and corrosion-resistant materials that could function as battery electrodes and
472 ion exchange membranes, energy-dense solid polymer fuels for autophagous systems, controllable
473 shape-morphing materials¹²⁹, and biocompatible materials that can be assembled into lightweight
474 composites composed of organic, inorganic, and even living matter. Advancements in additive
475 fabrication techniques across multiple scales, coupled with predictive (inverse) design will be
476 necessary to increase both the compositional and structural complexity of robots, and to realize
477 new levels of multifunctionality.

478
479 The tighter integration of sensing, actuation, control, and power towards biological size scales (i.e.,
480 organs and tissue) will realize first order improvements in robot autonomy. While synthetic
481 systems are striving to achieve tissue level autonomy, biohybrid ones already do. Consequently,
482 we expect research in this area to be fervently pursued in the immediate future. 3D printing will
483 also be an increasingly used tool; Direct Ink Writing,¹³⁰ PolyJet,¹³¹ and Digital Light
484 Processing^{132,133} have all been used to create complex robots with intricate internal networks out
485 of soft materials. The use of new, more energy dense materials will also provide new design tools
486 for directly printing robots. Finally, the direct chemical to mechanical conversion of energy, as
487 demonstrated with hydrocarbon fuels, will likely become increasingly used to provide the greater
488 energy densities and efficiencies required for biological magnitudes of endurance and adaptability.

489
490 Finally, the multifunctional energy storage paradigm we are attempting to codify can be further
491 separated into passive and active control. Within these logic mechanisms there is further
492 opportunity for multifunctionality; the structures themselves provide control (e.g., origami¹³⁴,
493 bistable beams^{135,136}, and elastomeric actuators¹³⁷⁻¹⁴⁰). In this context, information processing
494 becomes another material property embodied in the physics of the soft, architected structure,
495 enabling local computations that seamlessly integrate the sense-decide-response chain^{141,142}. For
496 example, networks of elastomeric light guides have demonstrated the information density and
497 sufficient sampling rates to classify deformation states through offboard neural network
498 training¹⁴³. Remarkably, the mechanical nonlinearity of elastomeric materials is even capable of
499 embodying recurrent neural network behavior; as demonstrated in the dynamics of a silicone
500 octopus arm¹⁴⁴. Embedded computation has the added benefit of requiring less energy, as the
501 information processing is inherently coupled to, or a by-product of, the deformation and
502 environmental loading. Embodied Energy and Embedded Computation, therefore, will be
503 intricately linked in the future of advanced robotics research.

504
505 The conjoined aspects of harvesting, storing, transforming, and releasing energy provide a unique
506 lens through which to view the evolution of autonomy and intelligence. Such considerations
507 similarly challenge roboticists to rethink how to design, program, and deploy their creations into
508 the world. The design principles that result from the proposed Embodied Energy paradigm have
509 the potential to yield new multifunctional energy storage systems that improve the multi-objective
510 optimization of robot endurance and adaptability. The frontier of this research lies in integrating
511 advancements in predictive multiscale design, multifunctional materials, digital manufacturing,
512 and robotics.

513
514

515 **References:**

516

517 1. Aubin, C. A. *et al.* Electrolytic vascular systems for energy-dense robots. *Nature* **571**, 51–
518 57 (2019).

519 **This paper details the development of a redox flow battery inspired multifunctional**
520 **energy storage system that uses a liquid electrolyte to simultaneously provide**
521 **electrical energy and hydraulic actuation to an untethered soft robotic fish.**

522 2. Shepherd, R. F. *et al.* Using explosions to power a soft robot. *Angew. Chemie - Int. Ed.* **52**,
523 2892–2896 (2013).

524 3. Wehner, M. *et al.* An integrated design and fabrication strategy for entirely soft,
525 autonomous robots. *Nature* **536**, 451–455 (2016).

526 **This work describes the creation of a fully autonomous soft robot that contains an**
527 **embedded microfluidic logic circuit and is powered by the catalytic decomposition of**
528 **an on-board monopropellant fuel.**

529 4. Ferreira, A. D. B. L., Nóvoa, P. R. O. & Marques, A. T. Multifunctional material systems:
530 A state-of-the-art review. *Compos. Struct.* **151**, 3–35 (2016).

531 **This review presents the state of the art in multifunctional material systems,**
532 **including recent advancements in structural materials used in energy storage**
533 **systems.**

534 5. Christodoulou, L. & Venables, J. D. Multifunctional material systems: The first
535 generation. *JOM* **55**, 39–45 (2003).

536 **This review discusses early research into multifunctional material systems, placing**
537 **some emphasis on materials used in energy storage implementations.**

538 6. Sakagami, Y., Watanabe, R. & Aoyama, C. The intelligent ASIMO: System overview and
539 integration. *IEEE/RSJ Intl. Conf. Intell. Robot. Syst.* **3**, 2478–2483 (2002).

540 7. Shepherd, R. F. *et al.* Multigait soft robot. *Proc. Natl. Acad. Sci.* **108**, 20400–20403.
541 (2011).

542 8. Gorissen, B. *et al.* Hardware sequencing of inflatable nonlinear actuators for autonomous
543 soft robots. *Adv. Mater.* **31**, (2019).

544 **This article describes an approach for embedding hardware intelligence into a robot**
545 **with multiple, nonlinear soft actuators, which are programmed via their structural**
546 **sequence and passive flow restrictors.**

547 9. Thomas, J. P. & Qidwai, M. A. The design and application of multifunctional structure-
548 battery materials systems. *JOM* **57**, 18–24 (2005).

549 10. Asp, L. E. & Greenhalgh, E. S. Structural power composites. *Compos. Sci. Technol.* **101**,
550 41–61 (2014).

551 11. Kim, T. H., Lee, S. J. & Choi, W. Design and control of the phase shift full bridge
552 converter for the on-board battery charger of electric forklifts. *J. Power Electron.* **12**, 113–
553 119 (2012).

554 12. Aglietti, G. S., Schwingshackl, C. W. & Roberts, S. C. Multifunctional structure
555 technologies for satellite applications. *Shock Vib. Dig.* **39**, 381–391 (2007).

556 13. Roberts, S. C. & Aglietti, G. S. Structural performance of a multifunctional spacecraft
557 structure based on plastic lithium-ion batteries. *Acta Astronaut.* **67**, 424–439 (2010).

558 14. Zhang, Y. *et al.* Multifunctional structural lithium-ion battery for electric vehicles. *J.*
559 *Intell. Mater. Syst. Struct.* **28**, 1603–1613 (2017).

560 15. Wang, M. *et al.* Biomorphic structural batteries for robotics. *Sci. Robot.* **5**, eaba1912

- 561 (2020).
- 562 16. Holness, A. E., Perez-rosado, A., Bruck, H. A., Peckerar, M. & Gupta, S. K.
563 Multifunctional wings with flexible batteries and solar cells for robotic birds. in
564 *Challenges in Mechanics of Time Dependent Materials, Volume 2* 155–162 (2017).
- 565 17. Bar-Cohen, Y. *Electroactive polymer (EAP) actuators as artificial muscles: reality,*
566 *potential, and challenges.* **136**, (SPIE press, 2004).
- 567 18. Kim, K. J. & Tadokoro, S. *Electroactive Polymers for Robotic Applications.* (Springer,
568 2007).
- 569 19. Duduta, M., Hajiesmaili, E., Zhao, H., Wood, R. J. & Clarke, D. R. Realizing the potential
570 of dielectric elastomer artificial muscles. *Proc. Natl. Acad. Sci.* **116**, 2476–2481 (2019).
- 571 20. Wang, T. *et al.* Electroactive polymers for sensing. *Interface Focus* **6**, 20160026 (2016).
- 572 21. Biddiss, E. & Chau, T. Electroactive polymeric sensors in hand prostheses: Bending
573 response of an ionic polymer metal composite. *Med. Eng. Phys.* **28**, 568–578 (2006).
- 574 22. Pelrine, R., Kornbluh, R., Pei, Q. & Joseph, J. High-speed electrically actuated elastomers
575 with strain greater than 100%. *Science* **287**, 836–839 (2000).
- 576 23. Anderson, I. A., Gisby, T. A., McKay, T. G., O’Brien, B. M. & Calius, E. P. Multi-
577 functional dielectric elastomer artificial muscles for soft and smart machines. *J. Appl.*
578 *Phys.* **112**, 041101 (2012).
- 579 24. Ji, X. *et al.* An autonomous untethered fast soft robotic insect driven by low-voltage
580 dielectric elastomer actuators. *Sci. Robot.* **4**, eaaz6451 (2019).
- 581 25. Li, T. *et al.* Agile and Resilient Insect-Scale Robot. *Soft Robot.* **6**, 133–141 (2019).
- 582 26. Shintake, J., Rosset, S., Schubert, B., Floreano, D. & Shea, H. Versatile soft grippers with
583 intrinsic electroadhesion based on multifunctional polymer actuators. *Adv. Mater.* **28**,
584 231–238 (2016).
- 585 27. Li, T. *et al.* Fast-moving soft electronic fish. *Sci. Adv.* **3**, 1–8 (2017).
- 586 28. Christianson, C., Goldberg, N. N., Deheyn, D. D., Cai, S. & Tolley, M. T. Translucent soft
587 robots driven by frameless fluid electrode dielectric elastomer actuators. *Sci. Robot.* **3**,
588 eaat1893 (2018).
- 589 29. Godaba, H., Li, J., Wang, Y. & Zhu, J. A soft jellyfish robot driven by a dielectric
590 elastomer actuator. *IEEE Robot. Autom. Lett.* **1**, 624–631 (2016).
- 591 30. Chen, Y., Zhao, H., Mao, J., Chirarattananon, P. & Helbling, E. F. Controlled flight of a
592 microrobot powered by soft artificial muscles. *Nature* **575**, 324–329 (2019).
- 593 31. Rothemund, P., Kellaris, N., Mitchell, S. K., Acome, E. & Keplinger, C. HASEL
594 Artificial Muscles for a New Generation of Lifelike Robots—Recent Progress and Future
595 Opportunities. *Adv. Mater.* **33**, 1–28 (2021).
- 596 32. Acome, E. *et al.* Hydraulically amplified self-healing electrostatic actuators with muscle-
597 like performance. *Science* **359**, 61–65 (2018).
- 598 33. Diteesawat, R. S., Helps, T., Taghavi, M. & Rossiter, J. Electro-pneumatic pumps for soft
599 robotics. *Sci. Robot.* **6**, eabc3721 (2021).
- 600 34. Kellaris, N., Venkata, V. G., Smith, G. M., Mitchell, S. K. & Keplinger, C. Peano-HASEL
601 actuators: Muscle-mimetic, electrohydraulic transducers that linearly contract on
602 activation. *Sci. Robot.* **3**, eaar3276 (2018).
- 603 35. Keplinger, C., Li, T., Baumgartner, R., Suo, Z. & Bauer, S. Harnessing snap-through
604 instability in soft dielectrics to achieve giant voltage-triggered deformation. *Soft Matter* **8**,
605 285–288 (2012).
- 606 36. Carrico, J. D., Kim, K. J. & Leang, K. K. 3D-Printed ionic polymer-metal composite soft

- 607 crawling robot. *IEEE Int. Conf. Robot. Autom.* 4313–4320 (2017).
- 608 37. Yeom, S. & Oh, I. A biomimetic jellyfish robot based on ionic polymer metal composite
609 actuators. *Smart Mater. Struct.* **18**, 085002 (2009).
- 610 38. Chen, Z., Um, T. I. & Bart-smith, H. Bio-inspired robotic manta ray powered by ionic
611 polymer–metal composite artificial muscles. *Int. J. Smart Nano Mater.* **3**, 296–308 (2012).
- 612 39. Fang, B., Ju, M. & Lin, C. K. A new approach to develop ionic polymer–metal composites
613 (IPMC) actuator: Fabrication and control for active catheter systems. *Sensors Actuators A
614 Phys.* **137**, 321–329 (2007).
- 615 40. Krishen, K. Space applications for ionic polymer-metal composite sensors, actuators, and
616 artificial muscles. *Acta Astronaut.* **64**, 1160–1166 (2009).
- 617 41. Shahinpoor, M. & Kim, K. J. Ionic polymer–metal composites: IV. Industrial and medical
618 applications. *Smart Mater. Struct.* **14**, 197–214 (2005).
- 619 42. Vallem, V., Sargolzaeiaval, Y., Ozturk, M., Lai, Y. C. & Dickey, M. D. Energy
620 Harvesting and Storage with Soft and Stretchable Materials. *Adv. Mater.* **33**, 2004832
621 (2021).
- 622 43. Hebner, R. & Beno, J. Flywheel Batteries Come Around Again. *IEEE Spectr.* **39**, 46–51
623 (2002).
- 624 44. Mousavi, S. M. G., Faraji, F., Majazi, A. & Al-haddad, K. A comprehensive review of
625 flywheel energy storage system technology. *Renew. Sustain. Energy Rev.* **67**, 477–490
626 (2017).
- 627 45. Fausz, J. L. & Richie, D. J. Flywheel simultaneous attitude control and energy storage
628 using a VSCMG configuration. *IEEE Int. Conf. Control Appl.* 991–995 (2000).
- 629 46. Polygerinos, B. P. *et al.* Soft robotics : Review of fluid-driven intrinsically soft devices ;
630 manufacturing , sensing , control , and applications in human-robot interaction. *Adv. Eng.
631 Mater.* **19**, 1700016 (2017).
- 632 47. Rus, D. & Tolley, M. T. Design, fabrication and control of soft robots. *Nature* **521**, 467–
633 475 (2015).
- 634 **This review explores recent advancements in the field of soft robots, including how**
635 **these robots can be fabricated, powered, and controlled.**
- 636 48. Rich, S. I., Wood, R. J. & Majidi, C. Untethered soft robotics. *Nat. Electron.* **1**, 102–112
637 (2018).
- 638 49. Tang, Y. *et al.* Leveraging elastic instabilities for amplified performance: Spine-inspired
639 high-speed and high-force soft robots. *Sci. Adv.* **6**, eaaz6912 (2020).
- 640 50. Gorissen, B., Melancon, D., Vasios, N., Torbati, M. & Bertoldi, K. Inflatable soft jumper
641 inspired by shell snapping. *Sci. Robot.* **5**, eabb1967 (2020).
- 642 51. Overvelde, J. T. B., Kloek, T., D’haen, J. J. A. & Bertoldi, K. Amplifying the response of
643 soft actuators by harnessing snap-through instabilities. *Proc. Natl. Acad. Sci.* **112**, 10863–
644 10868 (2015).
- 645 52. Forterre, Y., Skotheim, J. M., Dumais, J. & Mahadevan, L. How the Venus flytrap snaps.
646 *Nature* **433**, 421–425 (2005).
- 647 53. Pratt, G. A. & Williamson, M. M. Series Elastic Actuators. *Proceedings 1995 IEEE/RSJ
648 International Conference on Intelligent Robots and Systems. Human Robot Interaction
649 and Cooperative Robots* 399–406 (1995).
- 650 54. Seok, S. *et al.* Design principles for highly efficient quadrupeds and implementation on
651 the MIT Cheetah robot. *Proceedings - IEEE International Conference on Robotics and
652 Automation* 3307–3312 (2013).

- 653 55. Wehner, M. *et al.* Pneumatic energy sources for autonomous and wearable soft robotics.
654 *Soft Robot.* **1**, 263–273 (2014).
- 655 56. Tolley, M. T. *et al.* An untethered jumping soft robot. *IEEE/RSJ Int. Conf. Intell. Robot.*
656 *Syst.* 561–566 (2014).
- 657 57. Truby, R. L. & Li, S. Integrating chemical fuels and artificial muscles for untethered
658 microrobots. *Sci. Robot.* **5**, eabd7338 (2020).
- 659 58. Thomas, J. P., Qidwai, M. A. & Kellogg, J. C. Energy scavenging for small-scale
660 unmanned systems. *J. Power Sources* **159**, 1494–1509 (2006).
- 661 **This paper reviews different energy scavenging technologies, such as solar, thermal,**
662 **and wind, and models their relative effectiveness in increasing the edurance of**
663 **untethered, unmanned mechanical systems.**
- 664 59. Qidwai, M. A., Thomas, J. P., Kellogg, J. C. & Baucom, J. Energy harvesting concepts for
665 small electric unmanned systems. in *Smart Structures and Materials 2004: Active*
666 *Materials: Behavior and Mechanics* 84–95 (2004).
- 667 60. Joshi, P. *et al.* Autophagous spacecraft composite materials for orbital propulsion. in
668 *SPIE's 9th Annual International Symposium on Smart Structures and Materials* 171–179
669 (2002).
- 670 61. Chen, Z. *et al.* Balancing volumetric and gravimetric uptake in highly porous materials for
671 clean energy. *Science* **368**, 297–303 (2020).
- 672 62. Maeda, K., Shinoda, H. & Tsumori, F. Miniaturization of worm-type soft robot actuated
673 by magnetic field. *Jpn. J. Appl. Phys.* **59**, S11L04 (2020).
- 674 63. Do, T. N., Phan, H., Nguyen, T. & Visell, Y. Miniature Soft Electromagnetic Actuators
675 for Robotic Applications. *Adv. Funct. Mater.* **28**, 1–11 (2018).
- 676 64. Hines, L., Petersen, K., Lum, G. Z. & Sitti, M. Soft Actuators for Small-Scale Robotics.
677 *Adv. Mater.* **29**, 1603483 (2017).
- 678 65. Mao, G. *et al.* Soft electromagnetic actuators. *Sci. Adv.* **6**, eabc0251 (2020).
- 679 66. Li, J. *et al.* Development of a magnetic microrobot for carrying and delivering targeted
680 cells. *Sci. Robot.* **3**, eaat8829 (2018).
- 681 67. Peyer, K. E., Zhang, L. & Nelson, B. J. Bio-inspired magnetic swimming microrobots for
682 biomedical applications. *Nanoscale* **5**, 1259–1272 (2013).
- 683 68. Hu, W., Lum, G. Z., Mastrangeli, M. & Sitti, M. Small-scale soft-bodied robot with
684 multimodal locomotion. *Nature* **554**, 81–85 (2018).
- 685 69. Shen, W. & Zhu, S. Harvesting energy via electromagnetic damper: Application to bridge
686 stay cables. *J. Intell. Mater. Syst. Struct.* **26**, 3–19 (2015).
- 687 70. Asama, J., Burkhardt, M. R., Davoodi, F. & Burdick, J. W. Design Investigation of a
688 Coreless Tubular Linear Generator for a Moball: a Spherical Exploration Robot with
689 Wind-Energy Harvesting Capability. in *IEEE International Conference on Robotics and*
690 *Automation* 244–251 (IEEE, 2015).
- 691 71. Lazarus, N. & Meyer, C. D. Stretchable inductor with liquid magnetic core. *Mater. Res.*
692 *Express* **3**, 036103 (2016).
- 693 72. Lazarus, N., Meyer, C. D., Bedair, S. S., Slipper, G. A. & Kierzewski, I. M. Magnetic
694 elastomers for stretchable inductors. *ACS Appl. Mater. Interfaces* **7**, 10080–10084 (2015).
- 695 73. Jadhao, J. S. & Thombare, D. G. Review on Exhaust Gas Heat Recovery for I. C. Engine.
696 *Int. J. Eng. Innov. Technol.* **2**, 93–100 (2013).
- 697 74. Wang, E. H. *et al.* Study of working fluid selection of organic Rankine cycle (ORC) for
698 engine waste heat recovery. *Energy* **36**, 3406–3418 (2011).

- 699 75. Li, N. *et al.* New twist on artificial muscles. *Proc. Natl. Acad. Sci.* **115**, 11709–11716
700 (2018).
- 701 76. Kanik, M., Orguc, S., Varnavides, G. & Kim, J. Strain-programmable fiber-based artificial
702 muscle. *Science* **365**, 145–150 (2019).
- 703 77. Gao, W., de Ávila, B. E. F., Zhang, L. & Wang, J. Targeting and isolation of cancer cells
704 using micro/nanomotors. *Adv. Drug Deliv. Rev.* **125**, 94–101 (2018).
- 705 78. Li, D., Liu, C., Yang, Y., Wang, L. & Shen, Y. Micro-rocket robot with all-optic actuating
706 and tracking in blood. *Light Sci. Appl.* **9**, Article number: 84 (2020).
- 707 79. Behl, B. M., Razzaq, M. Y. & Lendlein, A. Multifunctional Shape-Memory Polymers.
708 *Adv. Mater.* **22**, 3388–3410 (2010).
- 709 80. Liu, C., Qin, H. & Mather, P. T. Review of progress in shape-memory polymers. *J. Mater.*
710 *Chem.* **17**, 1543–1558 (2007).
- 711 81. Lendlein, A., Behl, M., Hiebl, B. & Wischke, C. Shape-memory polymers as a technology
712 platform for biomedical applications. *Expert Rev. Med. Devices* **7**, 357–379 (2010).
- 713 82. Small, W., Metzger, M. F., Wilson, T. S. & Maitland, D. J. Laser-activated shape memory
714 polymer microactuator for thrombus removal following ischemic stroke: preliminary in
715 vitro analysis. *IEEE J. Sel. Top. QUANTUM Electron.* **11**, 892–901 (2005).
- 716 83. Chenal, T. P., Case, J. C., Paik, J. & Kramer, R. K. Variable stiffness fabrics with
717 embedded shape memory materials for wearable applications. in *IEEE/RSJ International*
718 *Conference on Intelligent Robots and Systems (IROS 2014)* 2827–2831 (IEEE, 2014).
- 719 84. Liu, R. *et al.* Shape memory polymers for body motion energy harvesting and self-
720 powered mechanosensing. *Adv. Mater.* **30**, 1705195 (2018).
- 721 85. Firouzeh, A., Salerno, M. & Paik, J. Stiffness control with shape memory polymer in
722 underactuated robotic origamis. *IEEE Trans. Robot.* **33**, 765–777 (2017).
- 723 86. Jin, B. *et al.* Programming a crystalline shape memory polymer network with thermo- and
724 photo-reversible bonds toward a single-component soft robot. *Sci. Adv.* **4**, 1–6 (2018).
- 725 87. Liu, Y., Du, H., Liu, L. & Leng, J. Shape memory polymers and their composites in
726 aerospace applications: a review. *Smart Mater. Struct.* **23**, 023001 (2014).
- 727 88. Bellin, I., Kelch, S. & Lendlein, A. Dual-shape properties of triple-shape polymer
728 networks with crystallizable network segments and grafted side chains. *J. Mater. Chem.*
729 **17**, 2885–2891 (2007).
- 730 89. Ze, Q., Kuang, X., Wu, S., Wong, J. & Montgomery, S. M. Magnetic shape memory
731 polymers with integrated multifunctional shape manipulations. *Adv. Mater.* **32**, 1906657
732 (2020).
- 733 90. Mohd Jani, J., Leary, M., Subic, A. & Gibson, M. A. A review of shape memory alloy
734 research, applications and opportunities. *Mater. Des.* **56**, 1078–1113 (2014).
- 735 91. Laschi, C. *et al.* Soft Robot Arm Inspired by the Octopus. *Adv. Robot.* **26**, 709–727
736 (2012).
- 737 92. Rodrigue, H., Wang, W., Han, M. & Kim, T. J. Y. An overview of shape memory alloy-
738 coupled actuators and robots. *Soft Robot.* **4**, 3–15 (2017).
- 739 93. Villanueva, A., Smith, C. & Priya, S. A biomimetic robotic jellyfish (Robojelly) actuated
740 by shape memory alloy. *Bioinspir. Biomim.* **6**, 036004 (2011).
- 741 94. Kim, H., Song, S. & Ahn, S. A turtle-like swimming robot using a smart soft composite
742 (SSC) structure. *Smart Mater. Struct.* **22**, 014007 (2013).
- 743 95. Koh, J. *et al.* Jumping on water: Surface tension–dominated jumping of water striders and
744 robotic insects. *Science* **349**, 517–522 (2015).

- 745 96. Jun, H. Y., Rediniotis, O. K. & Lagoudas, D. C. Development of a fuel-powered shape
746 memory alloy actuator system: II. Fabrication and testing. *Smart Mater. Struct.* **16**, S95
747 (2007).
- 748 97. Odhner, L. U. & Asada, H. H. Sensorless temperature estimation and control of shape
749 memory alloy actuators using thermoelectric devices. *IEEE/ASME Trans. Mechatronics*
750 **11**, 139–144 (2006).
- 751 98. Yang, X., Chang, L. & Pérez-arancibia, N. O. An 88-milligram insect-scale autonomous
752 crawling robot driven by a catalytic artificial muscle. *Sci. Robot.* **5**, eaba0015 (2020).
- 753 99. Kim, S. H. *et al.* Harvesting temperature fluctuations as electrical energy using torsional
754 and tensile polymer muscles. *Energy Environ. Sci.* **8**, 3336–3344 (2015).
- 755 100. Goguel, O. & PAO. TRIZ 40. Available at: http://www.triz40.com/TRIZ_GB.php.
756 (Accessed: 29th May 2021)
- 757 101. Mitcheson, B. P. D. *et al.* Human and machine motion for wireless electronic devices.
758 *Proc. IEEE* **96**, 1457–1486 (2008).
- 759 102. Johannisson, W. *et al.* A residual performance methodology to evaluate multifunctional
760 systems. *Multifunct. Mater.* **3**, 025002 (2020).
- 761 **This work discusses how the advantages of multifunctional systems over**
762 **monofunctional systems can be determined mathematically and leveraged to make**
763 **design decisions.**
- 764 103. Ragone, D. V. *Review of battery systems for electrically powered vehicles.* (SAE
765 Technical Paper, 1968).
- 766 104. Luo, X., Wang, J., Dooner, M. & Clarke, J. Overview of current development in electrical
767 energy storage technologies and the application potential in power system operation. *Appl.*
768 *Energy* **137**, 511–536 (2015).
- 769 105. Bossche, P. Van Den & Mierlo, J. Van. SUBAT: An assessment of sustainable battery
770 technology. *J. Power Sources* **162**, 913–919 (2006).
- 771 106. Madden, J. D. W. *et al.* Artificial muscle technology: physical principles and naval
772 prospects. *IEEE J. Ocean. Eng.* **29**, 706–728 (2004).
- 773 107. Alici, G. Softer is Harder : What Differentiates Soft Robotics from Hard Robotics ? *MRS*
774 *Adv.* **3**, 1557–1568 (2018).
- 775 108. Power-to-weight ratio - Wikipedia. Available at: https://en.wikipedia.org/wiki/Power-to-weight_ratio. (Accessed: 16th February 2021)
- 776 109. Boretti, A. A. Energy Recovery in Passenger Cars. *J. Energy Resour. Technol.* **134**,
777 022203 (2012).
- 778 110. Energy density - Wikipedia. Available at: https://en.wikipedia.org/wiki/Energy_density.
779 (Accessed: 16th February 2021)
- 780 111. Absolute Water Pumps - Water Pumps & Accessories. Available at:
781 <https://www.absolutewaterpumps.com/>. (Accessed: 16th February 2021)
- 782 112. Evans, J. Pump Efficiency—What Is Efficiency? (2012). Available at:
783 <https://www.pumpsandsystems.com/pump-efficiency-what-efficiency>. (Accessed: 16th
784 February 2021)
- 785 113. 9.4: Oxidation of Fatty Acids - Chemistry LibreTexts. Available at:
786 [https://chem.libretexts.org/Courses/Brevard_College/CHE_301_Biochemistry/09%3A_M
787 etabolism_of_Lipids/9.04%3A_Oxidation_of_Fatty_Acids](https://chem.libretexts.org/Courses/Brevard_College/CHE_301_Biochemistry/09%3A_Metabolism_of_Lipids/9.04%3A_Oxidation_of_Fatty_Acids). (Accessed: 16th February
788 2021)
- 789 114. Huber, J. E., Fleck, N. A. & Ashby, M. F. The selection of mechanical actuators based on
790

- 791 performance indices. *Proc. R. Soc. London. Ser. A Math. Phys. Eng. Sci.* **453**, 2185–2205
792 (1997).
- 793 115. Evans, A., Strezov, V. & Evans, T. J. Assessment of utility energy storage options for
794 increased renewable energy penetration. *Renew. Sustain. Energy Rev.* **16**, 4141–4147
795 (2012).
- 796 116. Love, L. J., Lanke, E. & Alles, P. *Estimating the impact (energy, emissions and*
797 *economics) of the U.S. fluid power industry.* (2012).
- 798 117. Balki, M. K., Sayin, C. & Canakci, M. The effect of different alcohol fuels on the
799 performance, emission and combustion characteristics of a gasoline engine. *Fuel* **115**,
800 901–906 (2014).
- 801 118. Peirs, J., Reynaerts, D. & Verplaetsen, F. Development of an axial microturbine for a
802 portable gas turbine generator. *J. Micromechanics Microengineering* **13**, 5–11 (2003).
- 803 119. Lefebvre, A. H. Fuel Effects on Gas Turbine Combustion — Ignition, Stability, and
804 Combustion Efficiency. *Trans. ASME* **107**, 24–37 (1985).
- 805 120. Liang, W., Liu, H., Wang, K. & Qian, Z. Comparative study of robotic artificial actuators
806 and biological muscle. *Adv. Mech. Eng.* **12**, 1–25 (2020).
- 807 121. Isermann, R. & Raab, U. Intelligent actuators — ways to autonomous actuating systems.
808 *Automatica* **29**, 1315–1331 (1993).
- 809 122. Veale, A. J. & Xie, S. Q. Towards compliant and wearable robotic orthoses: A review of
810 current and emerging actuator technologies. *Med. Eng. Phys.* **38**, 317–325 (2016).
- 811 123. Kedzierski, J., Holihan, E., Cabrera, R. & Weaver, I. Re-engineering artificial muscle with
812 microhydraulics. *Microsystems Nanoeng.* **3**, 17016 (2017).
- 813 124. Daerden, F. & Lefeber, D. Pneumatic artificial muscles: actuators for robotics and
814 automation. *Eur. J. Mech. Environ. Eng.* **47**, 11–21 (2002).
- 815 125. Chen, H., Ngoc, T., Yang, W., Tan, C. & Li, Y. Progress in electrical energy storage
816 system: A critical review. *Prog. Nat. Sci.* **19**, 291–312 (2009).
- 817 126. Sabihuddin, S., Kiprakis, A. E. & Mueller, M. A numerical and graphical review of
818 energy storage technologies. *energies* **8**, 172–216 (2015).
- 819 **This paper displays performance and statistical data for a wide range of modern**
820 **energy storage technologies, and also discusses their advantages and difficiencies**
821 **relative to each other.**
- 822 127. St. Pierre, R. & Bergbreiter, S. Toward autonomy in sub-gram terrestrial robots. *Annu.*
823 *Rev. Control. Robot. Auton. Syst.* **2**, 231–254 (2019).
- 824 128. Trimmer, W. S. N. Microrobots and micromechanical systems. *Sensors and Actuators* **19**,
825 267–287 (1989).
- 826 129. Johannisson, W., Harnden, R., Zenkert, D. & Lindbergh, G. Shape-morphing carbon fiber
827 composite using electrochemical actuation. *Proc. Natl. Acad. Sci.* **117**, 7658–7664 (2020).
- 828 130. Kotikian, A. *et al.* Untethered soft robotic matter with passive control of shape morphing
829 and propulsion. *Sci. Robot.* **4**, eaax7044 (2019).
- 830 131. Maccurdy, R., Katschmann, R., Kim, Y. & Rus, D. Printable hydraulics: A method for
831 fabricating robots by 3D co-printing solids and liquids. *2016 IEEE Int. Conf. Robot.*
832 *Autom.* 3878–3885 (2016).
- 833 132. Peele, B. N., Wallin, T. J., Zhao, H. & Shepherd, R. F. 3D printing antagonistic systems of
834 artificial muscle using projection stereolithography. *Bioinspir. Biomim.* **10**, 055003
835 (2015).
- 836 133. Wallin, T. J. *et al.* Click chemistry stereolithography for soft robots that self-heal. *J.*

- 837 *Mater. Chem. B* **5**, 6249–6255 (2017).
- 838 134. Treml, B., Gillman, A., Buskohl, P. & Vaia, R. Origami mechanologic. *Proc. Natl. Acad. Sci.* **115**, 6916–6921 | (2018).
- 839
- 840 135. Jiang, Y., Korpas, L. M. & Raney, J. R. Bifurcation-based embodied logic and
- 841 autonomous actuation. *Nat. Commun.* **10**, 128 (2019).
- 842 136. Song, Y. *et al.* Additively manufacturable micro-mechanical logic gates. *Nat. Commun.*
- 843 **10**, 882 (2019).
- 844 137. Preston, D. J. *et al.* Digital logic for soft devices. *Proc. Natl. Acad. Sci.* **116**, 7750–7759
- 845 (2019).
- 846 138. Chau, N., Slipher, G. A., Brien, B. M. O., Mrozek, R. A. & Anderson, I. A. A solid-state
- 847 dielectric elastomer switch for soft logic. *Appl. Phys. Lett.* **108**, 103506 (2016).
- 848 139. Wilson, K. E., Henke, E. M., Slipher, G. A. & Anderson, I. A. Rubbery logic gates.
- 849 *Extrem. Mech. Lett.* **9**, 188–194 (2016).
- 850 140. Henke, E.-F. M., Wilson, K. E., Slipher, G. A., Mrozek, R. A. & Anderson, I. A. Artificial
- 851 muscle logic devices for autonomous local control. in *Robotic Systems and Autonomous*
- 852 *Platforms: Advances in Materials and Manufacturing* 29–40 (Woodhead Publishing,
- 853 2019).
- 854 141. McEvoy, M. A. & Correll, N. Materials that couple sensing, actuation, computation, and
- 855 communication. *Science* **347**, 1261689 (2015).
- 856 142. Correll, N., Baughman, R., Voyles, R., Yao, L. & Inman, D. Robotic Materials. *arXiv*
- 857 *Prepr. arXiv1903.10480* (2019).
- 858 143. Van Meerbeek, I. M., De Sa, C. M. & Shepherd, R. F. Soft optoelectronic sensory foams
- 859 with proprioception. *Sci. Robot.* **3**, eaau2489 (2018).
- 860 144. Nakajima, K., Hauser, H., Li, T. & Pfeifer, R. Information processing via physical soft
- 861 body. *Sci. Rep.* **5**, 1–11 (2015).

862

863

864 **Figure Legends:**

865

866 **Fig. 1| Energy, control, and actuating systems in modern robots.** Energy storage elements are

867 highlighted in yellow, control elements are highlighted in green, and actuators are highlighted in

868 red for each robot. **a**, The ASIMO humanoid robot⁶. **b**, A multigait, quadrupedal soft robot

869 powered by a pneumatic tether⁷. **c**, An 8-degree-of-freedom walking robot with embedded

870 actuator sequencing and a single pneumatic input⁸. **d**, An untethered octopus-inspired robot

871 controlled by microfluidic logic and powered by the decomposition of a monopropellant fuel that

872 produces pneumatic actuation³. **e**, An untethered aquatic soft robot with a redox flow battery-

873 inspired vascular system that produces electrical energy and hydraulic actuation¹. **f**, The common

874 octopus. (*To provide a direct comparison with mobile robots **a–e**, we have highlighted the

875 primary actuators of the octopus: the tentacles. Note: There are secondary actuation and

876 sensory/control capabilities not depicted in this simplistic representation.)

877

878 **Fig 2| Energy storage and transduction form the framework of the Embodied Energy design**

879 **process.** The Embodied Energy technologies shown are created by storing a specific type of energy

880 into the structural or energy transduction components of a system. The images in the transduction

881 pathway depict, from left to right, an electric comb drive, a bistable mechanical actuator, a soft

882 combustion actuator, a magnetic solenoid actuator, and a thermally responsive gel. The variable

883 definitions are as follows: U = voltage, q = charge, H = magnetic field strength, B = magnetic flux
884 density, V = volume, S^0 = standard entropy, T = temperature, C = specific heat capacity, m = mass,
885 p = pressure, F = force, x = displacement, σ = mechanical stress, ϵ = strain. The acronyms are:
886 RFBs = redox flow batteries, SMES = superconducting magnetic energy storage, SHES = sensible
887 heat energy storage.

888
889 **Fig 3| Multifunctional Ragone plot of Embodied Energy storage and energy transducer**
890 **combinations.** Each pair of intersecting line segments (corresponding to a specific number and
891 color) represents the range of predicted energy density and predicted power density values for a
892 given energy storage and actuator combination, based on existing products and prototype
893 devices^{4,9,48,104–126}. Predicted energy density is the product of an energy source's energy density Z ,
894 efficiency α , and the efficiency η of the energy transducer where it is embodied. Predicted power
895 density is the product of an energy transducer's power density Γ , efficiency η , and the efficiency
896 α of the energy storage system in which it is embodied. [The intersection points of the line segment
897 pairs are arbitrarily chosen for visibility.]

898
899 **Extended Data Table 1| Energy density and power density of common energy storage and**
900 **actuator technologies**

901
902
903 **Supplementary Information:**

904
905 Supplementary information is available in the online version of this paper

906
907
908 **Acknowledgements:**

909
910 The authors thank the Office of Naval Research, Grant #N00014-20-1-2438, Air Force Office of
911 Scientific Research, Grant #FA9550-20-1-0254, and National Science Foundation, Grant
912 #EFMA-1830924

913
914
915 **Author Contributions:**

916
917 R.F.S. and J.A.L. conceived of the concept. C.A.A., J.A.L., and R.F.S. drafted key elements of
918 the manuscript. C.A.A. researched, collected, and analyzed data. C.A.A., B.G., and E.M. drafted
919 figures. P.R.B., N.L., G.A.S., C.K., J.B., and F.I. assisted in editing and refining the vision.

920
921
922 **Author Information**

923
924 Reprints and permissions information is available at www.nature.com/reprints. The authors
925 declare no competing financial interests. Correspondence and requests for materials should be
926 addressed to R.F.S. (rfs247@cornell.edu).